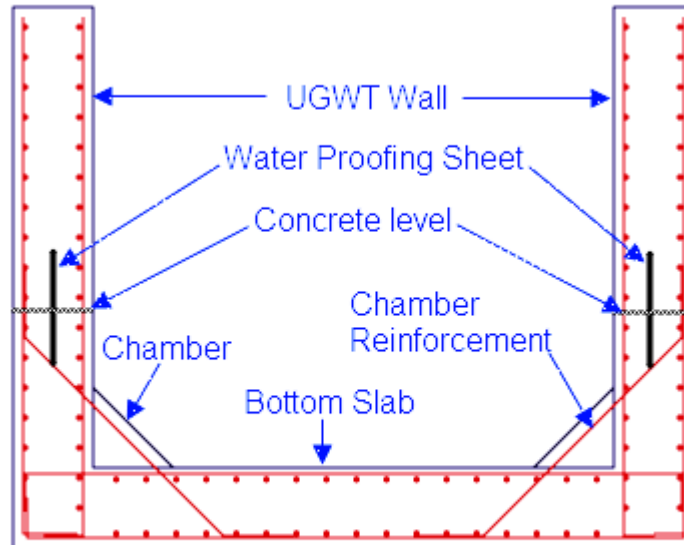


# DAMS & WATER RESOURCES ENGINEERING

## Design of Rectangular concrete Tank.

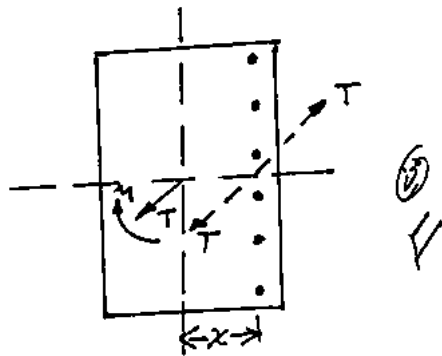
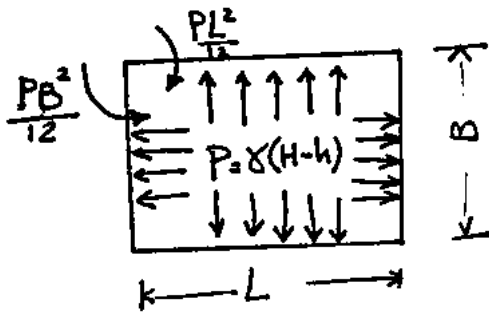
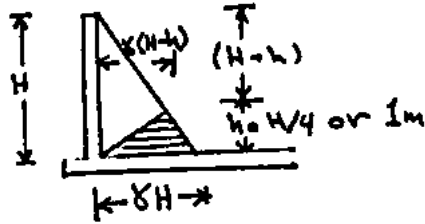


Under Ground Water Tank



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Approximate Design Method



(a) For tanks of ratio  $(4/B) \leq 2$

Referring to the Fig. below for the bottom height of  $h = H/4$  or  $1m$  (which ever is more), the bending is in vertical plane & this portion is designed as cantilever.

عندئذ الخزان بالسر ثابت الخزان تعرض الى انحناء Bending في الاتجاهين --



تدبركون هذا الانحناء افقي --

و تدبركون انحناء الراسي يكون شبيه cantilever ... الخزان الراسي الخزان.

\* يجب تدبر انبوه موزون الانحناءين  
في الخزان الراسي ان الخزان في تدبر موزون  
في انبوه موزون الراسي الخزان  
في انبوه موزون الراسي الخزان

The corners are designed for the maximum moment obtained after moment distribution with the intensity Pressure  $p = \gamma(H-h)$ .

In the absence of moment distribution the bending moment may be computed by the following approximate expression

Bending moment at centre of span =  $\left(\frac{PB^2}{16}\right)$  (producing

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Bending moment at ends of span =  $\left(\frac{PB^2}{12}\right)$  (producing tension on water face).

In addition to the bending moments, the walls are subjected to direct tension given by:-

Direct tension on long walls =  $T_L = \gamma(H-h) B/2$

Direct tension on short walls =  $T_b = \gamma(H-h) L/2$

Design moment =  $(M - T \cdot x)$

For B.M.,  $A_{st1} = \left[ \frac{M - T \cdot x}{f_{st} \cdot j \cdot d} \right]$

$\therefore A_{st} = (A_{st1} + A_{st2})$

For direct tension  $A_{st2} = (T / f_{st})$

(b) Ratio of  $(L/B) > 2$

In this case long walls are assumed to bend vertically & hence designed as cantilevers. Short walls are assumed to bend horizontally supported on long walls above  $H/4$  or  $1_m$  from bottom.

Bending moment for long walls =  $\left(\frac{\gamma H^3}{6}\right)$

B.M. for short walls (above  $1_m$  from base) =  $\frac{\gamma(H-h)B^2}{16}$

Maximum cantilever moment for short wall =  $\left(\frac{\gamma H h \cdot h}{2 \times 3}\right)$   
 $= \left(\frac{\gamma H \cdot h^2}{6}\right)$

In addition direct pulls are considered for long & short walls.

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A rectangular Reinforced Concrete water tank with an open top is required to store 80,000 liters of water. The inside dimensions of tank are 6m x 4m. The tank rests on walls on all the four sides. Design the side walls of the tank for the following data.

Free Board Board

$$F.B. = 15\text{cm}, j = 0.84, n = 13, f_c = 7\text{MPa}$$

$$f_{st} = 125\text{MPa (on faces away from water face)}, f_{st} = 100\text{MPa (on faces near water face)}$$

Solution :-

$$* \text{ Height of water} = \left( \frac{80,000 * 10^3}{600 * 400} \right) = 335\text{cm} = 3.35\text{m}$$

$$\text{Height of side walls} = (335 + 15) = 350\text{cm} = 3.5\text{m}$$

$$(L/B) = 6/4 = 1.5 < 2$$

∴ Walls designed as continuous slab subjected to water pressure above (H/4) or (1m) from bottom.

$$∴ P = \gamma(H-h) = (10 * 2.5) = 25\text{kN/m}^2$$

\* Moments in side walls:-

The moments in side walls is determined by moment distribution.

Fixed end moments:

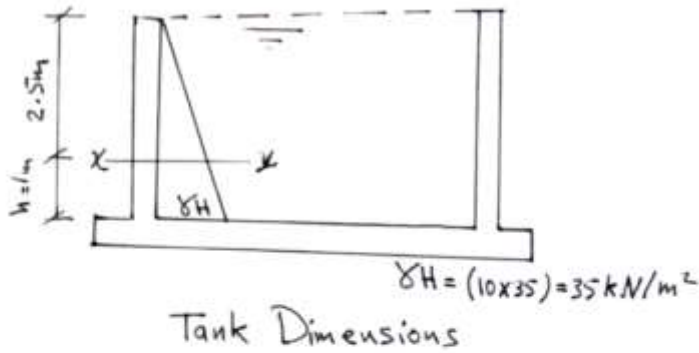
Long Walls

$$\left( \frac{P \cdot L^2}{12} \right) = \left( \frac{25 * 6^2}{12} \right) = 75\text{kN}\cdot\text{m}, \left( \frac{PB^2}{12} \right) = \left( \frac{25 * 4^2}{12} \right) = 34\text{kN}\cdot\text{m}$$

$$\left( \frac{P \cdot L^2}{8} \right) = \left( \frac{25 * 6^2}{8} \right) = 112.5\text{kN}\cdot\text{m}, \left( \frac{PB^2}{8} \right) = \left( \frac{25 * 4^2}{8} \right) = 50\text{kN}\cdot\text{m}$$

Short Walls

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	0.4		0.4	
	0.6		0.6	
+34	-75		+75	-34
+24.6	+16.4		-16.4	-24.6
+58.6	-58.6		+58.6	-58.6

$\frac{EI}{L}$ ,  $EI \rightarrow$  متساوية \*  
للجدارين

\* مختلف L

Distribution Stiffness Factor

DF

for Long wall

$$DF_{\text{Long wall}} = \frac{k}{2k} = \frac{\frac{EI}{6}}{\frac{EI}{6} + \frac{EI}{4}} = \frac{EI}{EI} \left( \frac{\frac{1}{6}}{\frac{4+6}{24}} \right)$$

$$DF_{\text{Long wall}} = \frac{4}{10} = 0.4$$

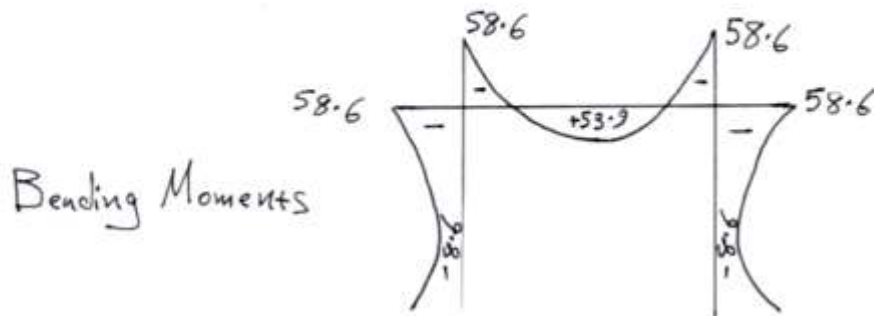
$$DF_{\text{short wall}} = \frac{\frac{EI}{4}}{\frac{EI}{4} + \frac{EI}{6}} = \frac{\frac{1}{4}}{\frac{10}{24}} = \frac{6}{10} = 0.6$$

Moment at support = 58.6 kN.m

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Moment at centre (Long walls) =  $(112.5 - 58.6) = 53.9 \text{ kN.m}$

Moment at centre (Short walls) =  $(50 - 58.6) = -8.6 \text{ kN.m}$



\* Design of Long & Short Walls :-

Maximum moment =  $58.6 \text{ kN.m}$

$$d_{req.} = \sqrt{\frac{M_{max}}{0.5 k_j b f_c}} \quad , \quad v = \frac{100}{7} = 14.286, \quad k = \frac{n}{n+r} = \frac{13}{13+14.3} = 0.476$$

$$d_{req.} = \sqrt{\frac{58.6 \times 10^6}{0.5 \times 0.476 \times 0.84 \times 1000 \times 7}} = 204.63 \text{ mm}$$

(at xx)

Adopt overall depth =  $250 \text{ mm}$

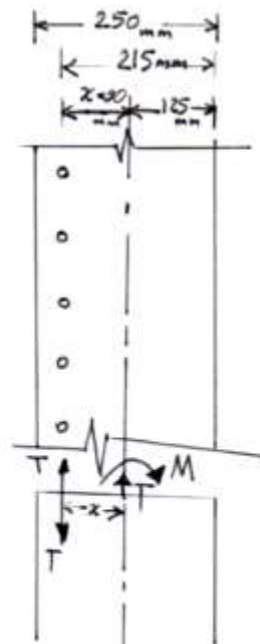
Use Effective depth =  $215 \text{ mm}$

Direct tension in long wall =  $T = \left(\frac{P \times B}{2}\right) = \left(\frac{25 \times 4}{2}\right) = 50 \text{ kN}$

Direct tension in short wall =  $T = \left(\frac{P \times L}{2}\right) = \left(\frac{25 \times 6}{2}\right)$

$$A_{st} (\text{Long wall corners}) = \left[ \frac{M - T \cdot x}{f_{st} \cdot j \cdot d} \right] + \frac{T}{f_{st}} \quad T = 75 \text{ kN}$$

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$$\text{Net Moment} = (M - T \cdot x)$$

T = Pull in steel

Fig. (Moments in Cross Section)

Referring to the Fig. above

$$\begin{aligned} \therefore A_{st} &= \left[ \frac{(58.6 \times 10^6) - (50 \times 10^3 \times 90)}{100 \times 0.84 \times 215} \right] + \left[ \frac{50 \times 10^3}{100} \right] \\ &= 3495 \text{ mm}^2 \end{aligned}$$

Use  $\phi$  20mm bar for reinforcement.

$$\text{Spacing of } 20\text{mm } \phi \text{ bars} = \frac{1000}{3495/314} \approx 90 \text{ mm/c}$$

- Center of Span (Long Walls)

$$A_{st} = \left[ \frac{(53.9 \times 10^6 - 50 \times 10^3 \times 90)}{125 \times 0.84 \times 215} \right] + \left[ \frac{50 \times 10^3}{125} \right] = 2588.26 \text{ mm}^2$$

## DAMS & WATER RESOURCES ENGINEERING

Half the bars from inner face at support are bent towards outer face at center providing an area of:  $\frac{3495}{2} = 1748 \text{ mm}^2$

For remaining area  $(2588 - 1748) = 840 \text{ mm}^2$

Provide  $\phi 16 \text{ mm}$  with spacing  $= \frac{1000}{840/201} = 239 \text{ mm/c}$

Use  $\phi 16 \text{ mm} @ 200 \text{ mm/c}$

Short Walls :- (corners)

$$A_{st} = \left[ \frac{(58.6 \times 10^6) - (75 \times 10^3 \times 90)}{100 \times 0.84 \times 215} \right] + \left( \frac{75 \times 10^3}{100} \right) = 3620 \text{ mm}^2$$

Use  $\phi 20 \text{ mm}$  with spacing  $= \frac{1000}{\frac{3620}{314}} = 86 \text{ mm/c}$

Use  $\phi 20 \text{ mm} @ 80 \text{ mm/c}$  (50% of bars bend towards outer face at center)

At the center of short walls

$$A_{st} = \left[ \frac{(-9 \times 10^6) - (75 \times 10^3 \times 90)}{100 \times 0.84 \times 215} \right] + \left( \frac{75 \times 10^3}{100} \right) = 122 \text{ mm}^2$$

$S = \frac{1000}{\frac{122}{314}} = 2573 \text{ mm/c}$   $\therefore$  (The bars which bends from the corner is enough)

• Design for Cantilever Moment (For 1m height from bottom).

$$\text{Cantilever moment} = (3.5 \times 10 \times \frac{1}{2} \times \frac{1}{3}) = 5.833 \text{ kN.m}$$

$$\therefore A_{st} = \left( \frac{5.833 \times 10^6}{100 \times 0.84 \times 215} \right) = 323 \text{ mm}^2$$



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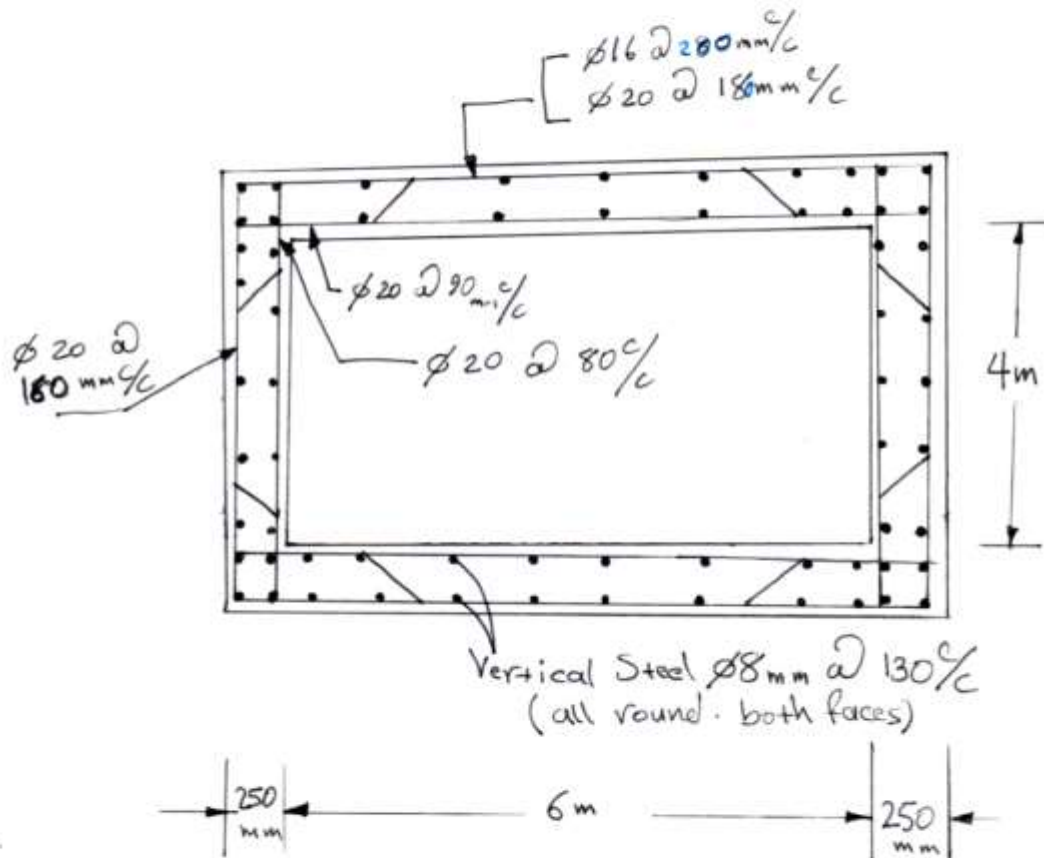
$$\text{Minimum steel} = 0.3\% = \left( \frac{0.3}{100} \times 10000 \times 250 \right) = 750 \text{ mm}^2$$

$$\text{Steel on each face} = \left( \frac{750}{2} \right) = 375 \text{ mm}^2$$

$$\text{Spacing of } 8 \text{ mm bars} = \left( \frac{1000}{\frac{375}{50}} \right) = 130 \text{ mm/c}$$

$$A_b = \left( \frac{\pi}{4} \times (8)^2 \right) = 50 \text{ mm}^2$$

Use  $\phi 8 \text{ mm/c}$  on both sides



Reinforcement Details in Water Tank (L/B < 2)