Operation and Safety of DamsDr. Ammar H. Kamel
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Example (2): determine the storage capacity for a reservoir according to the data in table, the uniform release is 18 cfs and average evaporation is 2 cfs (use TP or mass curve method)?

Month				Inflo	w		Outflow		
Anr.				141)		90		
May				310			92		
Jun				18			92		
Jul				56			93		
Aug				40			90		
Sep				135)		90		
Oct Now				100	•		90		
				85	-		89		
Jan				0			89		
	Feb			0			91		
	Mar	•		241	-		90		
	Apr	•		359			90		
	May	7		312			92		
	Jun Tul			/5			92		
	Aug	[82			93		
	Sep	•		247	1		90		
	Oct			198	}		90		
	Nov	,		268			90		
	Dec			266			89		
Sale	Jan			305)		89		
<u>S01:</u> Month	Inflow	Outflow	total	Inflow	Outflow	Cumulativa	Cumulativa	Difference	
MOIIIII	(of a)	(of a)	total		Valuma	$\int Cumulative inflow \Sigma It$	cumulative	Σ It Σ Ot	
	(CIS)	(015)	(of o)	Volume,	Ot(of	$\frac{11110}{(cf_{0} dov)}$	$\sum_{i=1}^{i} \sum_{j=1}^{i} \sum_{i=1}^{i} \sum_{j=1}^{i} \sum_{j$	$\sum_{i=1}^{n-2} \sum_{i=1}^{n-2} $	
			(CIS)	n(cis-uay)	Ot(CIS-	(CIS-day)	ZOT (CIS-	(cis-day)	
Apr	1/1	00	110	4220	2200	4220	2300	020	
Mov	210	90	110	4230	3300	4230	6772	7068	
Jun	19	92	112	<u> </u>	3472	13840	10122	/008	
Juli	10 56	92	112	1726	2502	14360	10132	4240	
Jui	30	93	113	1730	3303	10110	13033	2481	
Aug	40	90	110	1240	3410	1/330	1/045	311	
Sep	155	90	110	4050	3300	21406	20345	1061	
Oct	160	90	110	4960	3410	26366	23755	2611	
	221	89	109	6630	3270	32996	27025	5341	
Dec	85	89	109	2635	33/9	35631	30404	5227	
Jan	0	89	109	0	35/9	35631	35/83	1848	
Feb	0	91		0	3108	35631	36891	-1260	
Mar	241	90	110	7471	3410	43102	40301	2801	
Apr	359	90	110	10770	3300	53872	43601	10271	
May	312	92	112	9672	3472	63544	47073	16471	
Jun	75	92	112	2250	3360	65794	50433	15361	
Jul	50	93	113	1550	3503	67344	53936	13408	
Aug	82	93	113	2542	3390	69886	57326	12560	
Sep	247	90	110	7410	3300	77296	60626	16670	
Oct	198	90	110	6138	3410	83434	64036	19398	
Nov	268	90	110	8040	3300	91474	67336	24138	
Dec	266	89	109	8246	3379	99720	70715	29005	
Jan	305	89	109	9455	3379	109175	74094	35081	

Uniform release + evaporation=20 cfs



Storage Capacity=7068-(-1260)=8328cfs.day or 16490 acre.ft

Example (3): The following is a record of the mean monthly discharges of a river in a dry year. The available fall is 80 m. Determine

(1) The minimum capacity of a reservoir if the entire annual inflow is to be drawn off at a uniform rate (with no flow going into waste over the spillway).

(2) The amount of water must be initially stored to maintain the uniform draw off.

(3) The uniform power output assuming a plant efficiency of 70%.

(4) If the amount of water initially stored is 125 Mm3, the maximum possible draw off rate and the amount of water wasted over the spillway (assuming the same reservoir capacity determined in (i) above.

(5) If the largest reservoir that can be economically constructed is of capacity 125 Mm3, the maximum possible output and the amount of water wasted over the spillway.

(6) The capacity of the reservoir to produce 22.5 megawatts continuously throughout the year.

Month	Month Mean flow (cumec)		Mean flow (cumec)	
Jan.	29.7	July	68.0	
Feb.	75.3	Aug.	50.2	
March	66.8	Sept.	74.5	
April	57.2	Oct.	66.8	
May	23.2	Nov.	40.5	
June	26.3	Dec.	26.3	

<u>Sol:</u>

Take each month as 30 days for convenience; 1 month = 30 days \times 86400 sec = 2.592 \times 106 sec. Inflow volume in each month = monthly discharge \times 2.592 Mm3; and monthly inflow and cumulative inflow are tabulated in Table below:

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Month	Mean flow (cumec)	Inflow volume (Mm ³)	cumulative inflow (Mm ³)	Month	Mean flow (cumec)	Inflow volume (Mm ³)	cumulative inflow (Mm ³)
Jan.	29.7	77	77	July	68.0	176	897
Feb.	75.3	195	272	Aug.	50.2	130	1027
Mar.	66.8	173	445	Sept.	74.5	193	1220
April	57.2	148	593	Oct.	66.8	173	1393
May	23.2	60	653	Nov.	40.5	105	1498
June	26.3	68	721	Dec.	26.3	68	1566

Cumulative inflow into reservoir

Plot the mass curve of flow as cumulative inflow vs month as shown in Fig. below.



Mass curve studies in reservoir design (Example 1)

1. Join OA by a straight line; the slope of OA, *i.e.*, 1566 Mm3/yr or (1566×106) m³/ (365×86400)

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2. sec = 49.7 cumec is the uniform draw off throughout the year with no spill over the spillway. Draw $BC \parallel OA$, $GH \parallel OA$, B, G being the crests of the mass curve; EH = FGMinimum capacity of reservoir = DE + EH = 150 + 20 = 170 Mm3

Note: If the capacity is less than this, some water will be wasted and if it is more than this, the reservoir will never get filled up.

- 3. Amount of water to be initially stored for the uniform draw off of 49.7 cumec = $DE = 150 \text{ Mm}^3$
- 4. Continuous uniform power output in kW, $P = \frac{\rho_w gQH}{1000} * \eta_o$

Where

 $\rho w = mass density of water, 1000 kg/m3$

Q = discharge into turbines

H = head on turbines (\approx available fall)

 $\eta 0 = \text{overall or plant efficiency}$

$$P = \frac{\rho_w g Q H}{1000} * \eta_o \Rightarrow P = \frac{1000 * 9.81 * 49.7 * 80}{1000}$$

= 27400kW
= 27.4MW

- 5. If the amount of water initially stored is only 125 M.m³, measure DI = 125 M.m³, join *BI* and produce to *J*. The slope of the line *BJ* is the maximum possible draw off rate. Let the line *BJ* intersect the ordinate through *O* (*i.e.*, the cumulative inflow axis) at *K*. The vertical intercept *KJ'* = 1430 Mm³ and the slope of this line = 1430 Mm³/yr = 45.4 cumec which is the maximum possible draw off rate. To maintain the same reservoir capacity of 170 M.m³, draw the straight line HL || KJ intersecting the mass curve of flow at M and N. Draw the straight line GT || HL. The vertical intercept PM gives the amount of water wasted over the spillway (during the time period MN) which is 40 Mm³.
- 6. If the reservoir capacity is limited to 125 M.m3 from economic considerations, the line KJ intersects the mass curve of flow at R. Let the vertical at R meet the line GT (GT || KJ) at S. In this case the amount of water wasted over the spillway = RS = 85 Mm3. The maximum possible output in this case for a uniform draw off rate of 45.4 cumec is

$$P' = 27.4 \frac{45.4}{49.7} = 25MW$$

7. For a continuous power output of 22.5 MW the uniform draw off rate can be determined from the equation

$$22500kW = \frac{1000*9.81*Q*80}{1000}*0.7$$

= 40.8*cumec*

Which can also be calculated as $49.7 \times (22.5/27.4) = 40.8$ cumec = $40.8 (365 \times 86400 \text{ sec}) = 1287 \text{ Mm}^3/\text{yr}$. On the 1-year base, draw the ordinate at the end of December = 1287 M.m3 and join the line OQ (dashed line). The slope of this line gives the required draw off rate (40.8 cumec) to produce a uniform power output of 22.5 MW. Through B and D, i.e., the crest and the trough draw tangents parallel to the dashed line OQ (BV || OQ). The vertical intercept between the two tangents DZ gives the required capacity of the reservoir as 100 Mm3.

Reservoir Water Level:

- For short, deep reservoir, the reservoir water surface is level representing a reasonable assumption.
- If flow is passing the dam, there must be some slope to the water surface to cause this flow. When the cross sectional area of the reservoir is large compared with the rate of flow, the velocity will be small and the slope of the hydraulic grade line will be very flat.
- The computation of the water surface profile is an important part of reservoir design since it provides information on the water level at various points along the length of the reservoir from which the land requirements for the reservoir can be determined.

Acquisition of land or flowage rights over the land is necessary before the reservoir can be built. Docks, houses, storm drain outlets, roads, and bridge along the bank of the reservoir must be located above the maximum water level expected in the reservoir.

Recently, computer programs are widely used in reservoir and river modeling such as HEC-RAS, MIKE11, and MIKE21 as well as the geographic information system (GIS).

Storage in reservoir subject to marked backwater effects cannot be related to water surface elevation alone. A second parameter such as inflow rate or water surface elevation on a gage near upper end of the reservoir must also be used. Storage volume under each profile can be computed from cross sections by the methods used for earthwork computations.