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Case Two: Wall monolithic with the base.



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In this method some portion of the tank at the base acts as a cantilever & some load at the bottom is taken by the cantilever effect.

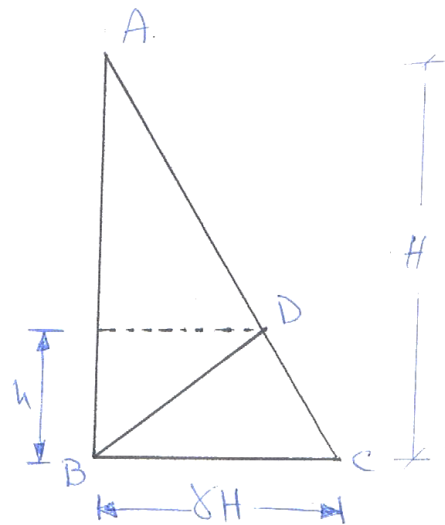
The cantilever effect depends on the dimensions of tank & the thickness of wall.

i- for $\frac{H^2}{D.t}$ is between 6 to 12

the value of $h = \frac{H}{3}$ or (1m) whichever ever is more.

ii- for $\frac{H^2}{D.t}$ is between

(12 to 30) the value $h = \frac{H}{4}$ or (1m) whichever is more.



Portion ABD is taken as Pressure causing hoop tension & DBC is taken as cantilever load.

The max. hoop tension occurs at D.

Example :- $H = 3.65\text{m}$, $D = 11.3\text{m}$, $t = 0.16\text{m}$

$$\frac{H^2}{D.t} = \frac{3.65^2}{11.3 \times 0.16} = 7.369 > 6$$

$$\therefore h = \frac{H}{3} = \frac{3.65}{3} = 1.22 > 1\text{m}$$

hence $h = 1.22\text{m}$

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Calculation for Reinforcement where the Hoop Force is Max:-

$$T = \frac{P(D)}{2} = \frac{10(3.65-1.22)}{2} \times 11.3 = 137.3 \text{ kN}$$

$$A_s = \frac{T}{f_s} = \frac{137.3 \times 10^3}{80.0} = 1716.25 \text{ mm}^2 \quad \text{Use } \phi 12 \text{ mm}$$

$$S = \frac{1000}{\left(\frac{1716.25}{\frac{\pi}{4} \times 12^2}\right)} = 65.89 \text{ mm} \%$$

Use $S = 130 \text{ mm} \%$ on both faces

Calculation of Max. B.M. :-

$$B.M._{\max} = \frac{1}{2} \gamma H \cdot h \cdot \frac{h}{3} = 9 \text{ kN}\cdot\text{m}$$

$$M = A_s f_s j d \implies d_{\text{eff}} = t - \left(\text{cover} + \frac{\phi}{2}\right)$$

$$d = 160 - \left(40 + \frac{12}{2}\right) = 114 \text{ mm} \quad 1160 - 1 \approx 1160 \text{ mm}^2$$

$$A_s = \frac{M}{f_s j d} = \frac{9 \times 10^6}{80 \times 0.85 \times 114} = \nearrow$$

Provide 12ϕ @ $97 \text{ mm} \%$ USE $\phi 12$ @ $90 \text{ mm} \%$

Nominal vertical reinforcement + s:

$$\frac{0.25}{100} \times 160 \times 1000 = 400 \text{ mm}^2$$

Provide $\frac{1000}{\left(\frac{400}{\frac{\pi}{4} \times 12^2}\right)} = 282.74 \text{ mm} \%$
Use $560 \text{ mm} \%$ in each face.

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Ex. :- Design a circular tank with fixed base, for a capacity of 400m^3 . The depth of water is to be 4.5m , including a free-board of 25cm . $f_c = 9\text{N/mm}^2$, $f_{ct} = 1.2\text{N/mm}^2$, $n = 9$, $f_s = 80\text{N/mm}^2$. Bearing Capacity of soil = 70 kN/m^2 .

Solution :- effective depth = $4.5 - 0.25 = 4.25\text{m}$

$$\frac{\pi}{4} D^2 \times 4.25 = 400\text{m}^3$$

$$D = 10.95 \text{ Use } D = 11.0\text{m}$$

$$t_{\min} = ? \quad T = \frac{1}{2} \gamma h D = \frac{1}{2} \times 10 \times 4.5 \times 11 = 247\text{ kN/m}$$

$$A_{st} = \frac{T}{f_{st}} = \frac{247 \times 1000}{80} = 3094\text{mm}^2$$

$$t_{\min} = \frac{1}{1000} \left[\frac{T}{f_{ct}} - (n-1) A_{st} \right] ; n = \frac{E_s}{E_c} = \frac{200 \times 10^3}{4700 \sqrt{f_c}} \approx 15.1$$

$$= \frac{1}{1000} \left[\frac{247 \times 1000}{1.2} - (9-1) \times 3094 \right]$$

$$= 181\text{mm} \text{ use } t = 185\text{mm}$$

$$\frac{H^2}{Dt} = \frac{(4.25)^2}{11 \times 0.185} = 8.876 \text{ (between 6-12)}$$

$$\therefore \frac{4.250}{3} = 1.4166 > 1\text{m}$$

$$\therefore h = 1.416\text{m}$$

Design of Walls for hoop tension :-

$$\text{Max. hoop tension} = \frac{\gamma (H-h) D}{2} = \frac{10 (4.25 - 1.42) \times 11}{2} = 155.65\text{ kN}$$

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Area of steel

$$A_s = \frac{I}{f_s} = \frac{155.65 \times 10^3}{80} = 1945.625 \text{ mm}^2$$

Use $\phi 12 \text{ mm}$ $A_b = 113 \text{ mm}^2$

$$S = \frac{1000}{1946/113} = 58 \sim 60 \text{ mm} \%$$

for both faces use $\delta = 120 \text{ mm} \%$

Design for Cantilever Action:-

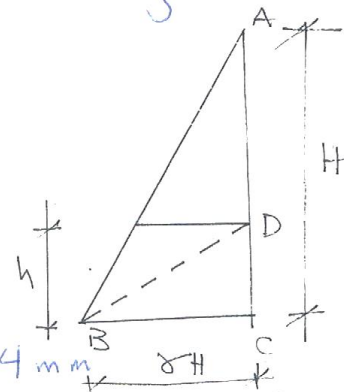
$$M_{\max} = \frac{1}{2} \gamma H \cdot h \cdot \frac{h}{3} = \frac{1}{2} \times 10 \times 4.25 \times 1.42 \times \frac{1.42}{3} = 14.28 \text{ kNm/m}$$

$$M = \frac{1}{2} f_c k d b j d$$

$$k = \frac{n}{n+r} = \frac{9}{9+80} = 0.5$$

$$j = 1 - \frac{k}{3} = 1 - \frac{0.5}{3} = 0.83$$

$$d = \left(\frac{2 \times 14.28 \times 10^6}{9 \times 0.5 \times 1000 \times 0.83} \right)^{\frac{1}{2}} = 87.44 \text{ mm}$$



Thickness of the wall $t = 87.44 + 40 + \frac{12}{2} = 133.44 \text{ mm} < 185 \text{ mm}$
OK

$$M = A_s f_s j d \Rightarrow A_s = \frac{M}{f_s j d} = \frac{14.28 \times 10^6}{80 \times 0.83 \times (185 - (40 + 6))} = 1547 \text{ mm}^2 \text{ /m}$$

$$S = \frac{1000}{1547/113} = 73 \text{ mm} \%$$

use $\phi 12 \text{ mm}$ $\phi 70 \text{ mm} \%$

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nominal Vertical Reinforcement = $(0.2 - 0.3)\%$ of gross concrete area:-

$$\text{Use } 0.3\% \Rightarrow A_{s \text{ secondary}} = \frac{0.3}{100} * 185 * 1000 = 555 \text{ mm}^2/\text{m}'$$

$$\text{for two faces } A_s = \frac{555}{2} = 277.5 \text{ mm}^2/\text{m}'$$

$$S = \frac{1000}{277.5/113} = 407.2 \Rightarrow \text{use } S = 400 \text{ mm/c for both faces.}$$

Design of Base Slab :-

Critical case when tank is empty

$$\begin{aligned} \text{Load from wall} &= \pi (11 + 0.185) * 4.5 * 0.185 * 24 \\ &= 644.28 \text{ kN} \end{aligned}$$

$$\text{Intensity of soil Pressure} = \frac{644.28}{\frac{\pi}{4} * (12.34)^2} = 5.39 \text{ kN/m}^2$$

$$\text{Max. B.M.} = \frac{3}{16} q$$