## Shearing Stress

Forces parallel to the area resisting the force cause shearing stress. It differs to tensile and compressive stresses, which are caused by forces perpendicular to the area on which they act. Shearing stress is also known as tangential stress.

$$
\tau=\frac{V}{A}
$$

where V is the resultant shearing force which passes which passes through the centroid of the area A being sheared.


Double Shear

## SOLVED PROBLEMS IN SHEARING STRESS

## Problem 115

What force is required to punch a 20 -mm-diameter hole in a plate that is 25 mm thick?
The shear strength is $350 \mathrm{MN} / \mathrm{m}^{2}$.

## Solution 115



The resisting area is the shaded area along the perimeter and the shear force $V$ is equal to the punching force $P$.

$$
\begin{aligned}
V & =\tau A \\
P & =350[\pi(20)(25)] \\
& =549778.7 \mathrm{~N} \\
& =549.8 \mathrm{kN}
\end{aligned}
$$

## Problem 116

As in Fig. 1-11c, a hole is to be punched out of a plate having a shearing strength of 40 ksi . The compressive stress in the punch is limited to 50 ksi . (a) Compute the maximum thickness of plate in which a hole 2.5 inches in diameter can be punched. (b) If the plate is 0.25 inch thick, determine the diameter of the smallest hole that can be punched.

## Solution 116

(a) Maximum thickness of plate:

Based on puncher strength:


Figure 1-11c

$$
\begin{aligned}
& \qquad \begin{aligned}
& P=\sigma A \\
&=50\left[\frac{1}{4} \pi\left(2.5^{2}\right)\right] \\
&=78.125 \pi \text { kips } \rightarrow \text { Equivalent shear force of the plate } \\
& \text { Based on shear strength of plate: } \\
& V=\tau \mathrm{A} \quad \rightarrow \mathrm{~V}=\mathrm{P} \\
& 78.125 \pi=40[\pi(2.5 t)] \\
& t=0.781 \text { inch }
\end{aligned}
\end{aligned}
$$

(b) Diameter of smallest hole:

Based on compression of puncher:

$$
\begin{aligned}
P & =\sigma A \\
& =50\left(\frac{1}{4} \pi d^{2}\right) \quad \\
& =12.5 \pi d^{2} \quad \rightarrow \text { Equivalent shear force for plate }
\end{aligned}
$$

Based on shearing of plate:

```
\(V=\tau A \quad \rightarrow \mathrm{~V}=\mathrm{p}\)
    \(12.5 \pi d^{2}=40[\pi d(0.25)]\)
    \(d=0.8 \mathrm{in}\)
```


## Problem 117

Find the smallest diameter bolt that can be used in the clevis shown in Fig. $1-11 \mathrm{~b}$ if $\mathrm{P}=$ 400 kN . The shearing strength of the bolt is 300 MPa .

## Solution 117



## Problem 118

A 200-mm-diameter pulley is prevented from rotating relative to 60 -mm-diameter shaft by a $70-\mathrm{mm}$-long key, as shown in Fig. P -118. If a torque $\mathrm{T}=2.2 \mathrm{kN} \cdot \mathrm{m}$ is applied to the shaft, determine the width $b$ if the allowable shearing stress in the key is 60 MPa .


Solution 118


## Problem 119

Compute the shearing stress in the pin at $B$ for the member supported as shown in Fig. $\mathrm{P}-119$. The pin diameter is 20 mm .


Figure P-119

Solution 119


## Problem 120

The members of the structure in Fig. P-120 weigh $200 \mathrm{lb} / \mathrm{ft}$. Determine the smallest diameter pin that can be used at A if the shearing stress is limited to 5000 psi. Assume single shear.


Solution 120
For member $A B$ :
Length, $L_{A B}=\sqrt{4^{2}+4^{2}}$

$$
=5.66 \mathrm{ft}
$$



FBD of member


FBD of member BC

$$
\begin{aligned}
& \text { Weight, } \left.\begin{array}{rl}
W_{A B} & =5.66(200) \\
& =1132 \mathrm{lb} \\
\Sigma M_{A}=0 \\
4 R_{B H}+4 R_{B V} & =2 W_{A B} \\
4 R_{B H}+4 R_{B V} & =2(1132) \\
R_{B H}+R_{B V}=566 \quad \rightarrow \text { (1) }
\end{array} . \begin{array}{rl}
\end{array}\right)
\end{aligned}
$$

For member $B C$ :

$$
\text { Length, } \begin{aligned}
L_{B C} & =\sqrt{3^{2}+6^{2}} \\
& =6.71 \mathrm{ft} \\
\text { Weight, } W_{B C} & =6.71(200) \\
& =1342 \mathrm{lb}
\end{aligned}
$$

$$
\Sigma M_{C}=0
$$

$$
6 R_{B H}=1.5 W_{B C}+3 R_{B V}
$$

$$
6 R_{B H}-3 R_{B V}=1.5(1342)
$$

$$
2 R_{B H}-R_{B V}=671 \quad \rightarrow(2)
$$

Add equations (1) and (2)

$$
R_{B H}+R_{B V}=566 \quad \rightarrow(1)
$$

$$
\frac{2 R_{B H}-R_{B V}=671}{3 R_{N W}}=1237 \quad \rightarrow(2)
$$

$$
R_{B H}=412.33 \mathrm{lb}
$$

From equation (1):

$$
412.33+R_{B V}=566
$$

$$
R_{B V}=153.67 \mathrm{lb}
$$

From the FBD of member $A B$

$$
\Sigma F_{H}=0
$$

$$
R_{A H}=R_{B H}=412.33 \mathrm{lb}
$$

$$
\Sigma F_{V}=0
$$

$$
R_{A V}+R_{B V}=W_{A B}
$$

$$
R_{A V}+153.67=1132
$$

$$
R_{A V}=978.33 \mathrm{lb}
$$

$$
\begin{aligned}
& R_{A}=\sqrt{R_{A H}^{2}+R_{A V}^{2}} \\
&=\sqrt{412.33^{2}+978.33^{2}} \\
&=1061.67 \mathrm{lb} \rightarrow \text { shear force of pin at } \mathrm{A} \\
& V=\tau A \\
& 1061.67=5000\left(\frac{1}{4} \pi d^{2}\right) \\
& d=0.520 \mathrm{in}
\end{aligned}
$$

## Problem 121

Referring to Fig. P-121, compute the maximum force $P$ that can be applied by the machine operator, if the shearing stress in the pin at $B$ and the axial stress in the control rod at C are limited to 4000 psi and 5000 psi, respectively. The diameters are 0.25 inch for the pin, and 0.5 inch for the control rod. Assume single shear for the pin at B.


Solution 121

$$
\begin{aligned}
& {\left[\Sigma M_{B}=0\right] \quad 6 P=2 T \sin 10^{\circ} \rightarrow(1)} \\
& {\left[\Sigma F_{H}=0\right] \quad B_{H}=T \cos 10^{\circ} \rightarrow \text { from (1), } \mathrm{T}=3 \mathrm{P} / \sin 10^{\circ}} \\
& B_{H}=\left(3 P / \sin 10^{\circ}\right) \cos 10^{\circ} \\
& B_{H}=3 \cot 10^{\circ} \mathrm{P} \\
& {\left[\Sigma F_{V}=0\right] \quad B_{V}=T \sin 10^{\circ}+P \rightarrow \text { from (1), } T \sin 10^{\circ}=3 \mathrm{P}} \\
& B_{V}=3 P+P \\
& B_{V}=4 P \\
& R_{B}{ }^{2}=B_{H}{ }^{2}+B_{V}{ }^{2} \\
& R_{B}{ }^{2}=\left(3 \cot 10^{\circ} P\right)^{2}+(4 P)^{2} \\
& R_{B}{ }^{2}=305.47 P^{2} \\
& R_{B}=17.48 \mathrm{P} \\
& P=R_{B} / 17.48 \rightarrow(2)
\end{aligned}
$$

Based on tension of rod (equation 1):

$$
\begin{aligned}
& P=\frac{1}{3} T \sin 10^{\circ} \\
& P=\frac{1}{3}\left[5000 \times \frac{1}{4} \pi(0.5)^{2}\right] \sin 10^{\circ} \\
& P=56.83 \mathrm{lb}
\end{aligned}
$$

Based on shear of rivet (equation 2):
$P=4000 \times \frac{1}{4} \pi(0.25)^{2} / 17.48$
$P=11.23 \mathrm{lb}$
Safe load $P=11.23 \mathrm{lb}$

## Problem 122

Two blocks of wood, width $w$ and thickness $t$, are glued together along the joint inclined at the angle $\theta$ as shown in Fig. P-122. Using the free-body diagram concept in Fig. 1-4a, show that the shearing stress on the glued joint is $\tau=P \sin 2 \theta / 2 A$, where $A$ is the crosssectional area.


Figure 1-4a Normal and shear components of the resultant on arbitrary section.


Figure P-122

Solution 122


Problem 123
A rectangular piece of wood, 50 mm by 100 mm in cross section, is used as a compression block shown in Fig. $\mathrm{P}-123$. Determine the axial force P that can be safely applied to the block if the compressive stress in wood is limited to $20 \mathrm{MN} / \mathrm{m}^{2}$ and the shearing stress parallel to the grain is limited to $5 \mathrm{MN} / \mathrm{m}^{2}$. The grain makes an angle of $20^{\circ}$ with the horizontal, as shown. (Hint: Use the results in Problem 122.)

## Solution 123

Based on maximum compressive stress:
Normal force:

$$
N=P \cos 20^{\circ}
$$

Normal area:


$$
\begin{aligned}
& A_{N}=50\left(100 \mathrm{sec} 20^{\circ}\right) \\
&=5320.89 \mathrm{~mm}^{2} \\
& N=\sigma A_{N} \\
& P \cos 20^{\circ}=20(5320.89) \\
& P=113247 \mathrm{~N} \\
&=133.25 \mathrm{kN}
\end{aligned}
$$

Based on maximum shearing stress:
Shear force:
$V=P \sin 20^{\circ}$

$$
\begin{aligned}
& \text { Shear area: } \\
& \begin{aligned}
& A_{V}=A_{N} \\
&=5320.89 \mathrm{~mm}^{2} \\
& V=\tau A_{V} \\
& P \sin 20^{\circ}=5(5320.89) \\
& P=77786 \mathrm{~N} \\
&=77.79 \mathrm{kN}
\end{aligned}
\end{aligned}
$$

For safe compressive force, use $P=77.79 \mathrm{kN}$

## Bearing Stress

Bearing stress is the contact pressure between the separate bodies. It differs from compressive stress, as it is an internal stress caused by compressive forces.


$$
\sigma_{b}=\frac{P_{b}}{A_{b}}
$$

## SOLVED PROBLEMS IN BEARING STRESS

## Problem 125

In Fig. 1-12, assume that a $20-\mathrm{mm}$-diameter rivet joins the plates that are each 110 mm wide. The allowable stresses are 120 MPa for bearing in the plate material and 60 MPa for shearing of rivet. Determine (a) the minimum thickness of each plate; and (b) the largest average tensile stress in the plates.


Figure 1-12

## Solution 125

(a) From shearing of rivet:

$$
\begin{aligned}
P & =\tau A_{\text {rivets }} \\
& =60\left[\frac{1}{4} \pi\left(20^{2}\right)\right] \\
& =6000 \pi \mathrm{~N}
\end{aligned}
$$

From bearing of plate material:
$P=\sigma_{b} A_{b}$
$6000 \pi=120(20 t)$
$t=7.85 \mathrm{~mm}$
(b) Largest average tensile stress in the plate:
$P=\sigma A$
$6000 \pi=\sigma[7.85(110-20)]$
$\sigma=26.67 \mathrm{MPa}$

## Problem 126

The lap joint shown in Fig. P-126 is fastened by four $3 / 4$-in.-diameter rivets. Calculate the maximum safe load $P$ that can be applied if the shearing stress in the rivets is limited to 14 ksi and the bearing stress in the plates is limited to 18 ksi . Assume the applied load is uniformly distributed among the four rivets.


## Solution 126

Based on shearing of rivets:
$P=\tau A$
$P=14\left[4\left(\frac{1}{4} \pi\right)\left(\frac{3}{4}\right)^{2}\right]$
$P=24.74 \mathrm{kips}$

Based on bearing of plates:
$P=\sigma_{b} A_{b}$
$P=18\left[4\left(\frac{3}{4}\right)\left(\frac{7}{8}\right)\right]$
$P=47.25 \mathrm{kips}$
Safe load $P=\mathbf{2 4 . 7 4} \mathrm{kips}$

## Problem 127

In the clevis shown in Fig. 1-11b, find the minimum bolt diameter and the minimum thickness of each yoke that will support a load $P=14$ kips without exceeding a shearing stress of 12 ksi and a bearing stress of 20 ksi .


Figure 1-11b

