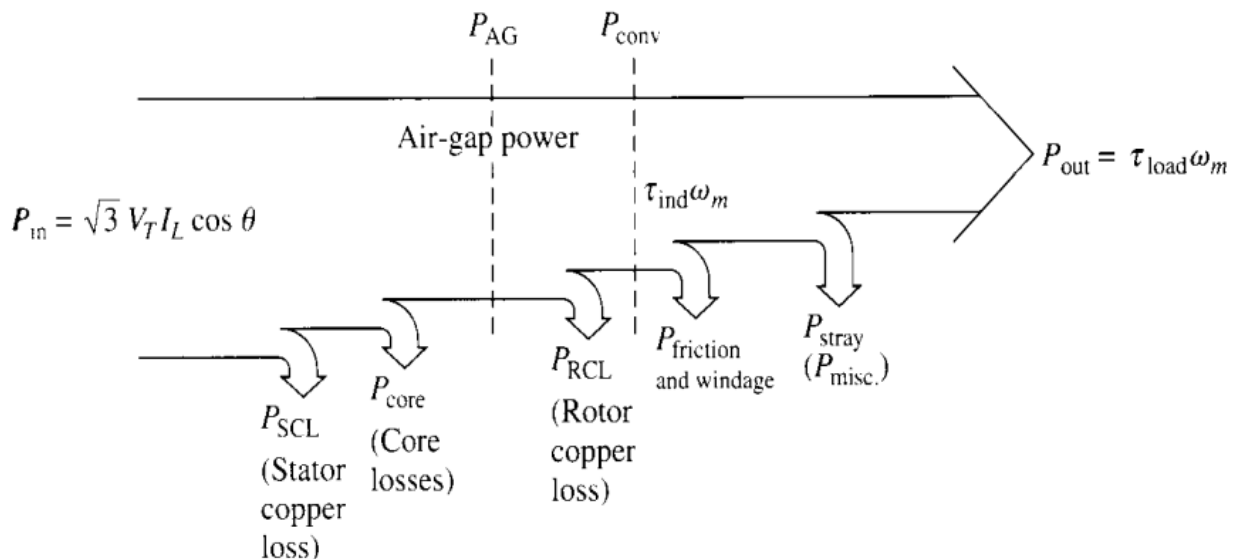




2-8 Power and Energy Diagram: -



$$P_1 = m_1 I_1 V_1 \cos \theta_1 = 3 I_1 V_1 \cos \theta_1 = \sqrt{3} I_L V_L \cos \theta_1$$

$$P_M = I_2 e^2 R_{\mu} = I_2 e^2 R_2 e \frac{1-s}{s}, I_2 e = \frac{E_2 e}{Z_2 e s}$$

$$P_M = E_2 e (1-s) I_2 e \frac{R_2 e}{Z_2 e} = (1-s) I_2 e E_2 e \cos \theta_2 e$$

Since $\frac{R_2 e / s}{Z_2 e}$

$$P_M = I_2 e E_2 e \cos \theta_2 e - s E_2 e I_2 e \cos \theta_2 e = P_{em} - P_{cu2}$$

$$P_M = P_{em} - s P_{em} = (1-s) P_{em}$$

$$P_{cu2} = I_2 e^2 R_2 e = \frac{E_2 e}{Z_2 e} I_2 e R_2 e = E_2 e I_2 e \frac{R_2 e}{Z_2 e s}$$

$$= s E_2 e I_2 e \frac{R_2 e}{Z_2 e s} = s E_2 e I_2 e \cos \theta_2 e$$

$$P_{em} = P_M + P_{cu2} = I_2 e^2 \frac{R_2 e}{s} = I_2 e^2 \left(R_2 e + R_2 e \frac{1-s}{s} \right) = \frac{P_{cu2}}{s}$$

$$P_2 = P_M - (P_{fw} + P_{add}); P_{em} = P_1 - P_{cu1} - P_{fe}$$

$$P_M = P_{em} - P_{cu2} = P_1 - P_{cu1} - P_{fe} - P_{cu2}$$



$$P_2 = P_1 - (P_{cu1} + P_{cu2} + P_{fe} + P_{fw} + P_{add})$$

$$T_{em} = \frac{P_{em}}{\omega_1} = \frac{60}{2\pi n_s} P_{em} = \frac{P}{2\pi F_1} P_{em}$$

$$T_{em} = \frac{P_M}{\omega_2} = \frac{60}{2\pi n} P_M = \frac{P}{2\pi F_2} P_M$$

$$P_{cu2} = P_{em} - P_M = T_{em}(\omega_1 - \omega_2) = s(\omega_1 T_{em}) = sP_{em}$$

$$\text{Where: } s = \frac{\omega_1 - \omega_2}{\omega_1}$$

$$T_{em} = \frac{P_{cu2}}{s\omega_1}, \quad s = \frac{P_{cu2}}{\omega_1 T_{em}} = \frac{P_{cu2}}{P_{em}} = \frac{I_2^2 R_2}{I_2^2 R_2 / s}$$

$$P_M = I_2^2 R_2 \frac{1-s}{s} = P_{cu2} \frac{1-s}{s} = sP_{em} \left(\frac{1-s}{s} \right) = (1-s)P_{em}$$

Ex1) A 3-phase, 4-pole, 50 Hz IM, the impedance of the star connected rotor winding is $(0.2 + j3)\Omega$ per phase the no-load induced emf between slip-rings is 220 V, find the rotor current and power factor at rated.

Sol:

$$n_1 = n_s = \frac{60F}{P} = \frac{60 \times 50}{2} = \frac{3000}{2} = 1500 \text{ rpm}$$

$$s = \frac{n_1 - n}{n_1} = \frac{1500 - 1455}{1500} = 0.03$$

$$E_2 = \frac{220}{\sqrt{3}} = 127 \text{ V}$$

$$E_2 s = sE_2 = 0.03 \times 127 = 3.81 \text{ V}$$

$$Z_2 s = \sqrt{R_2^2 + (sX_2)^2} = \sqrt{0.2^2 + (0.03 \times 3)^2} = 0.22 \Omega$$

$$I_2 = \frac{E_2 s}{Z_2 s} = \frac{3.81}{0.22} = 17.32 \text{ A}$$

$$\cos \theta_2 = \frac{R_2}{Z_2} = \frac{0.2}{0.22} = 0.909$$



Ex2) A 3-phase ,4-pole,380v,50HZ IM with rotor impedance of $(0.1+j0.6) \Omega/\text{phase}$, both winding is λ -connected with $T1/T2=1.5$. find the stator current if the excitation current is $(1-j10) \text{ A}$, and motor speed is 1440 rpm, neglect the primary impedance($Z1=0$)

SOL:

$$n1 = \frac{60F1}{P} = 1500 \text{rpm}, s = \frac{1500 - 1440}{1500} = 0.04$$

$$R2e = 0.1 \times 1.5^2 = 0.225 \Omega, X2e = 0.6 \times 1.5^2 = 1.35 \Omega$$

$$Vphas = \frac{Vline}{\sqrt{3}} = \frac{380}{\sqrt{3}} = 220 \text{v}, Z2e = \frac{R2e}{s} + jX2e = \frac{0.225}{0.04} + j1.35$$

$$I2e = \frac{v}{z2e} = \frac{220}{5.625 + j1.35} = 37 - j8.87 \text{A}$$

$$I1 = Ie + I2e = (1 - j10) + (37 - j8.87) = 38 - j18.87$$

$$I1 = 42.43$$

Ex3) A3-phase ,6-pole,440v ,50HZ IM. the parameters of its star connected winding are, $R1=R2e=0.1$, $X1=X2e=0.4$, $Ye=0.008-j0.06 \Omega/\text{phase}$. find the current and power factor at 50% the rated load at which the slip is 0.04. use the exact equivalent cct.

Sol:

$$Rm = R2e \frac{1-s}{s} = 0.1 \frac{1-0.04}{0.04} = 2.4 \Omega$$

$$Vp = \frac{440}{\sqrt{3}} = 254 \text{v}$$

$$y2e = \frac{1}{z2e} = \frac{1}{2.5 + j0.4} = 0.39 - j0.06$$

$$yab = ye + y2e = (0.008 - j0.06) + (0.39 + j0.06) = 0.398 - j0.66$$

$$Zab = \frac{1}{yab} = \frac{1}{0.398 - j0.66} = \frac{0.398 - j0.66}{0.398^2 - 0.66^2} = 0.67 + j1.11$$

$$Zt = Z1 + Zab = (0.1 + j0.4) + (0.67 + j1.11) = 0.77 + j1.51$$

$$I1 = \frac{Vphase}{Zt} = \frac{254}{0.77 + j1.51} = 68 - j133.5$$



$$I_1 = 150A, \cos \theta_1 = \frac{I_a}{I_1} = \frac{68}{150} = 0.45$$

Ex4) A 3-phase, 4-pole, 50Hz IM, at full-load delivers, $T_2=120\text{N.M}$ torque at 0.03slip. find the efficiency if the total stator losses are $(0.1P_2)$ and $P_{fw}=0.01P_2$

Sol:

$$n_1 = n_s = \frac{60F_1}{P} = \frac{60 \times 50}{2} = 1500 \text{ rpm}$$

$$s = \frac{n_1 - n}{n_1} = \frac{1500 - n}{1500} = 0.03 \rightarrow n = 1455 \text{ rpm}$$

$$\text{or } n = (1 - s)n_1 = (1 - 0.03) \times 1500 = 1455 \text{ rpm}$$

The useful output power is

$$P_2 = \omega \cdot T = \frac{2\pi n}{60} \times T_2 = 2\pi \frac{1455}{60} \times 120 = 18275 \omega$$

$$P_\mu = P_2 + P_{fw} = 1.01P_2 = 1.01 \times 18275 = 18458 \omega$$

$$P_{em} = P_\mu \frac{n_1}{n} = 18458 \times \frac{1500}{1455} = 19029$$

$$\text{or } P_{em} = \frac{P_\mu}{1 - s} = \frac{18458}{1 - 0.03} = 19029 \omega$$

The total input power to the motor is :

$$P_1 = P_{em} + P_{stator} = 19029 + 0.1 \times 18275 = 20932 \omega$$

And efficiency

$$\eta = \frac{18275}{20932} = \frac{P_2}{P_1}$$