

Ex. 1 Design the slabs of the building showing below. $L.L = 3 \text{ kN/m}^2$, The additive dead load (Finishing & Tiling) equal to 2 kN/m^2 , $f_c' = 30 \text{ MPa}$, $f_y = 400 \text{ MPa}$. Find the magnitude of loads which applied from the slabs on the beam B_1 .

Solution -
1 - Thickness of the slab.

$$h \geq \left\{ \begin{array}{l} \frac{P}{180} = \frac{2(6000 + 7500)}{180} = 150 \text{ mm} \\ 90 \text{ mm} \end{array} \right.$$

\therefore Use $h = 150 \text{ mm}$

2 - Calculate the design loads:-

$$D.L. = 0.15 \times 1 \times 1 \times 24 + 2 = 5.6 \text{ kN/m}^2$$

$$W_u = 1.2(5.6) + 1.6(3) = 11.52 \text{ kN/m}^2$$

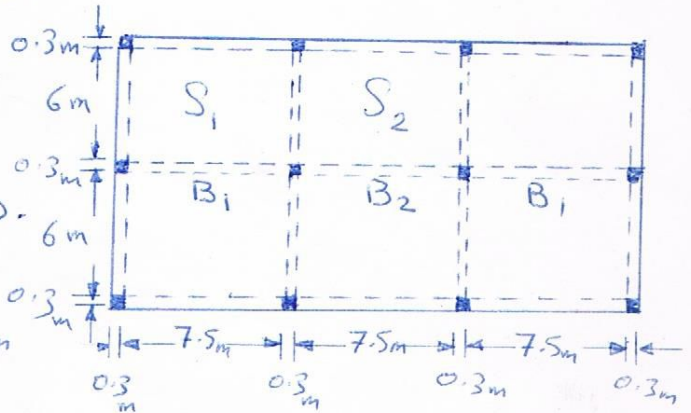
3 - Check the thickness of slab according to shear requirements.

$$d = 150 - 20 - 6 = 124 \text{ mm}$$

$$V_{ud} = 11.52 \left(\frac{6}{2} - 0.124 \right) = 35.13 \text{ kN}$$

$$\phi V_c = \frac{0.75}{6} \sqrt{30} \times 1000 \times 124 \times 10^{-3} = 84.9 \text{ kN}$$

$\therefore V_{ud} < \phi V_c \implies \therefore$ the thickness is adequate for shear



4- Max. & Min. ratios of Steel Reinforcement:

$$P_{max} = (0.85)^2 * \frac{30 * 0.003}{400 * 0.003 + 0.004}, E_t = 0.004 = 0.02322$$

$$A_{smin} = 0.0018bh = 0.0018 * 1000 * 150 = 270 \text{ mm}^2/\text{m}$$

5- Calculating of BMs .

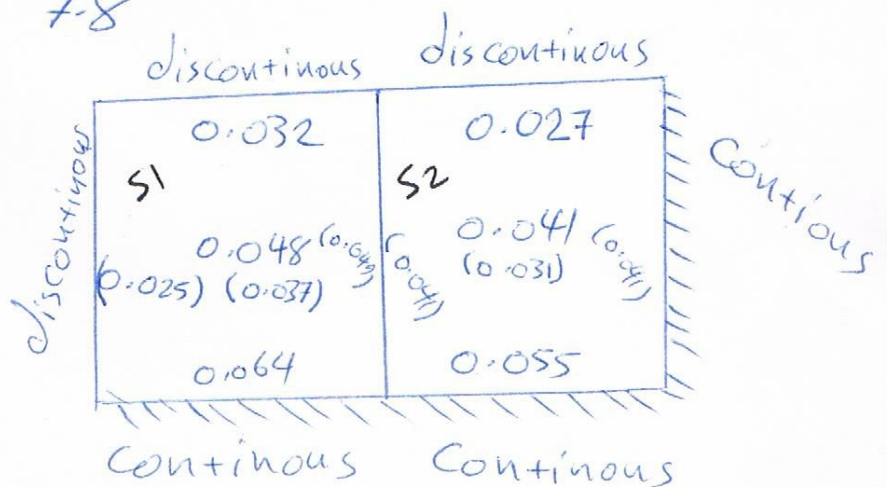
$$S \leq \begin{cases} \text{c/c of short span length} = 6 + 0.3 = 6.3 \text{ m} \\ \text{clear length of short span} + 2h = 6 + 2 * 0.15 = 6.3 \text{ m} \end{cases}$$

take the smallest value $\therefore S = 6.3 \text{ m}$

$$L \leq \begin{cases} 7.5 + 0.3 = 7.8 \text{ m} \\ 7.5 + 2 * 0.15 = 7.8 \text{ m} \end{cases}$$

$$\therefore L = 7.8 \text{ m}$$

$$m = \frac{6.3}{7.8} = 0.808$$



* Bending Moments in short direction
- Slab S1

$$M_{u\text{disc}}^- = 0.032 * 11.52 * 6.3^2 = 0.032 * 457.23 = 14.63 \text{ kN}\cdot\text{m/m}$$

$$M_{u\text{disc}}^+ = 0.048 * 457.23 = 21.95 \text{ kN}\cdot\text{m/m}$$

$$M_{u\text{cont}}^- = 0.064 * 457.23 = 29.26 \text{ kN}\cdot\text{m/m}$$

- Slab S2

$$M_{u\text{disc}}^- = 0.027 * 457.23 = 12.35 \text{ kN}\cdot\text{m/m}$$

$$M_{u\text{disc}}^+ = 0.041 * 457.23 = 18.75 \text{ kN}\cdot\text{m/m}$$

$$M_{u\text{cont}}^- = 0.055 * 457.23 = 25.15 \text{ kN}\cdot\text{m/m}$$

* Bending Moments in long direction.

- Slab S1

$$M_{u\text{disc}}^- = 0.025 * 457.23 = 11.43 \text{ kN}\cdot\text{m/m}$$

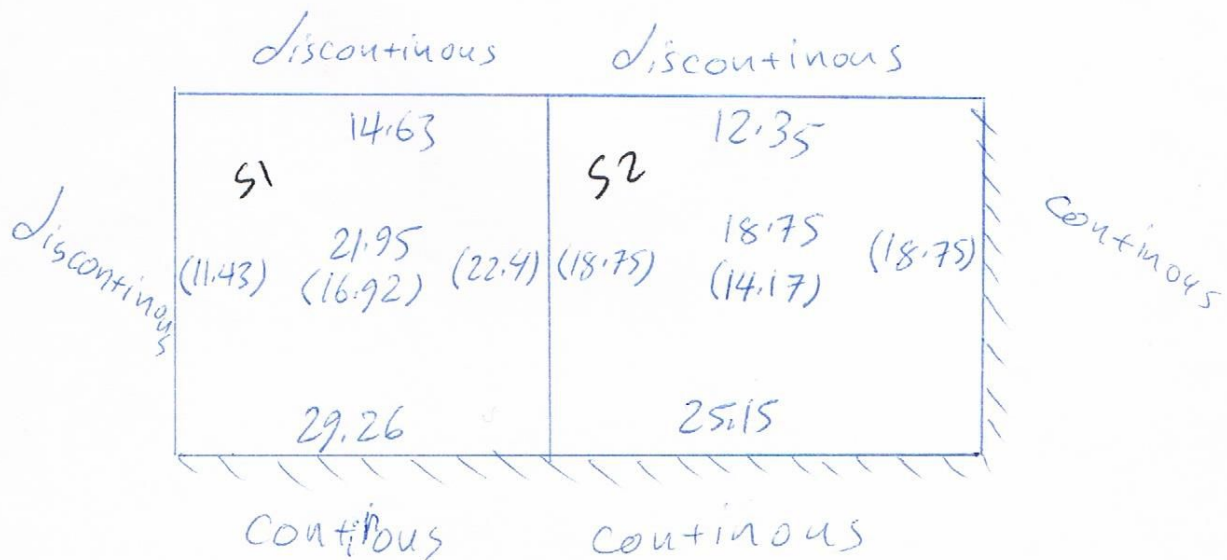
$$M_{u\text{disc}}^+ = 0.037 * 457.23 = 16.92 \text{ kN}\cdot\text{m/m}$$

$$M_{u\text{cont}}^- = 0.049 * 457.23 = 22.4 \text{ kN}\cdot\text{m/m}$$

- Slab S2

$$M_{u\text{cont}}^- = 0.041 * 457.23 = 18.75 \text{ kN}\cdot\text{m/m}$$

$$M_{u\text{disc}}^+ = 0.031 * 457.23 = 14.17 \text{ kN}\cdot\text{m/m}$$



Steel Reinforcement

a- Short Direction:-

$$k = \frac{M_u}{f_c' b d^2}, \omega = \rho \frac{f_y}{f_c'}, \rho = \text{From Table (p4)}$$

$$k = \frac{M_u}{\phi f_c' b d^2}$$

Reinforcement for middle strip in short direction (SI)

Moment	k	ω	ρ	$A_s = \rho b d$	A_s Provided	A_s added
$M_u^+ = 21.95$	0.053	0.055	0.00413	512	$\phi 10/150$ (526)	—
$M_u^-_{disc.} = 14.63$	0.035	0.036	0.0027	335	$\phi 10/300$ (263)	$\phi 8/300$ (167)
$M_u^-_{con.} = 29.26$	0.070	0.074	0.0056	695	$\phi 10/150$ (526)	$\phi 10/300$ (263)

$$\rho_{max} = 0.0232, \rho_t = 0.0203, A_{smin} = 0.0026bh$$

$$A_{smin} = 0.00180 * 1000 * 150 = 270.0 \text{ mm}^2/\text{m}$$

* All ρ value $< \rho_{max} = 0.0232 \therefore o.k.$

* All ρ value $< \rho_t = 0.0203 \implies \phi = 0.9$

* All $A_s > A_{smin} =$

$$S = \frac{1000}{A_s / A_b} = \frac{1000 * 79}{512} = 154 \text{ mm}$$

$$\text{Use } S = 150 \text{ mm } \phi$$

50% of bars will be bend & then ($A_{s \text{ provided}}$) is found

$$A_s = \frac{1000}{5} A_b$$

Reinforcement for middle strip in short direction (S_2)

Moment	K	ω	ρ	$A_s = \rho b d$ <small>mm²</small>	A_s provided <small>mm²</small>	A_s add. <small>mm²</small>
$M_u^+ = 18.75$	0.045	0.047	0.0035	434	$\phi 10/180$ (438)	—
$M_u^-_{disc.} = 12.35$	0.030	0.031	0.0023	286	$\phi 10/360$ (219)	$\phi 8/360$ (139)
$M_u^-_{con.} = 25.15$	0.060	0.063	0.0047	583	$\phi 10/180$ (438)	$\phi 10/360$ (219)

All value of ρ & A_s is ok for $\rho_{max.}$, ρ_t & $A_{s_{min.}}$

— for vertical strip the steel reinforcement = $\frac{2}{3}$ of steel reinforcement for middle strip.

* Spacing of vertical strip = $1.5 * S$ of middle strip.

* S must not be more than $(2h)$.

* A_s for vertical strip $\geq A_{s_{min.}}$

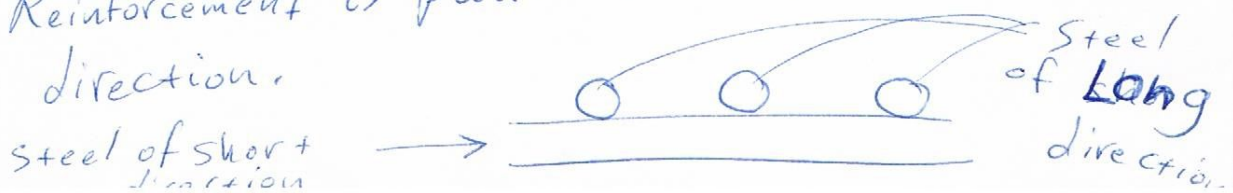
* In practical case A_s vertical strip = A_s middle strip

in that case there are lost in steel reinforcement.

— Steel Reinforcement in Long Direction —

$$d = h - (1.5d_b + 20) = 150 - (1.5 * 12 + 20) = 112 \text{ mm}$$

This Reinforcement is putted on the steel of short direction.



Reinforcement of Long Direction.

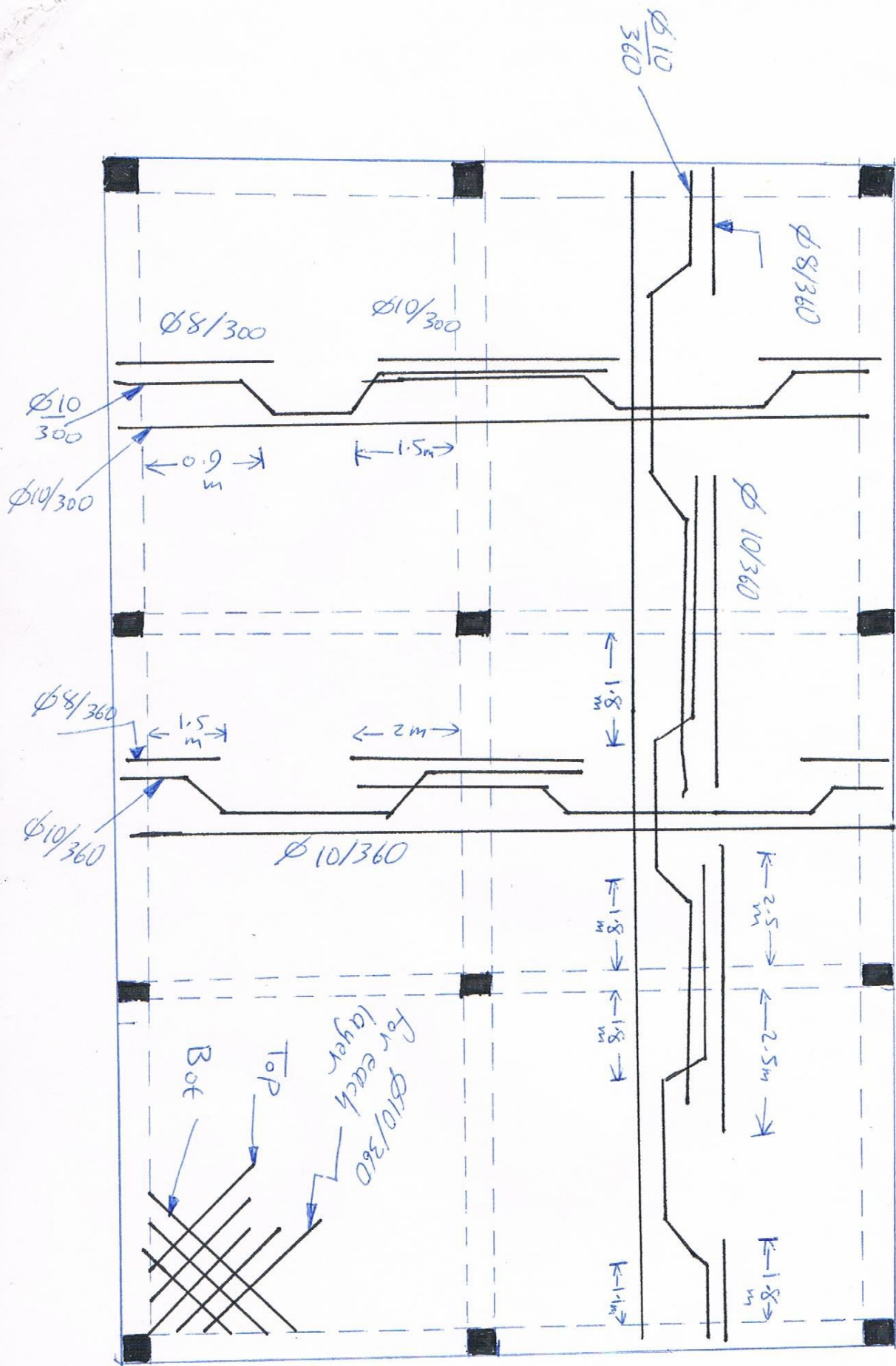
Moment kN.m	k	ω	ρ	$A_s = \rho b d$	A_s provided	A_s add.
$M_u^+ = 16.92$	0.05	0.052	0.0039	437	$\phi 10/80$ (438)	—
$M_u^-_{disc} = 11.43$	0.034	0.035	0.0026	292	$\phi 10/360$ (219)	$\phi 8/360$ (139)
$M_u^-_{con} = 22.4$	0.066	0.069	0.0052	583	$\phi 10/80$ (438)	$\phi 10/360$ (219)

* For Torsion Reinforcement the same diameters & spacing of Positive Reinforcement in short direction can be used.

- The load which applied on beam (B₁) equal to:-

$$W_e = \frac{W_s}{3} \frac{(3-m^2)}{2} = \frac{11.52 \times 6.3}{3} \frac{(3-0.8^2)}{2} \times 2 = 57 \text{ kN/m}$$

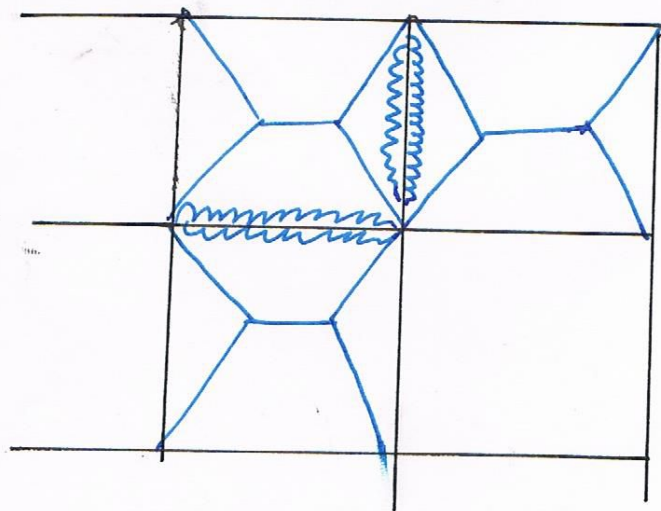
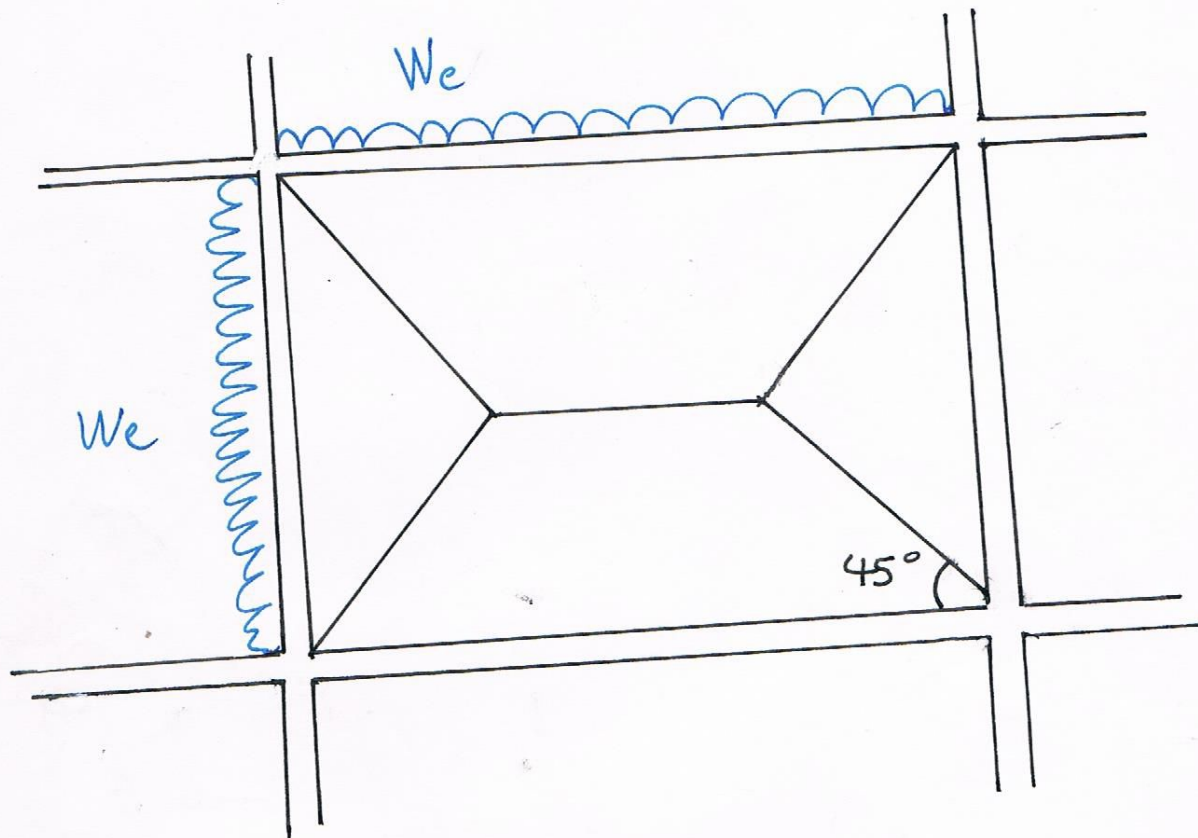
* Torsion Reinforcement must put for every corner.



W equivalent

$$W_e(\text{for short beams}) = \frac{W_u S}{3}$$

$$W_e(\text{for Long beams}) = \frac{W_u S}{3} \left(\frac{3 - m^2}{2} \right)$$



Torsion Reinforcement:-

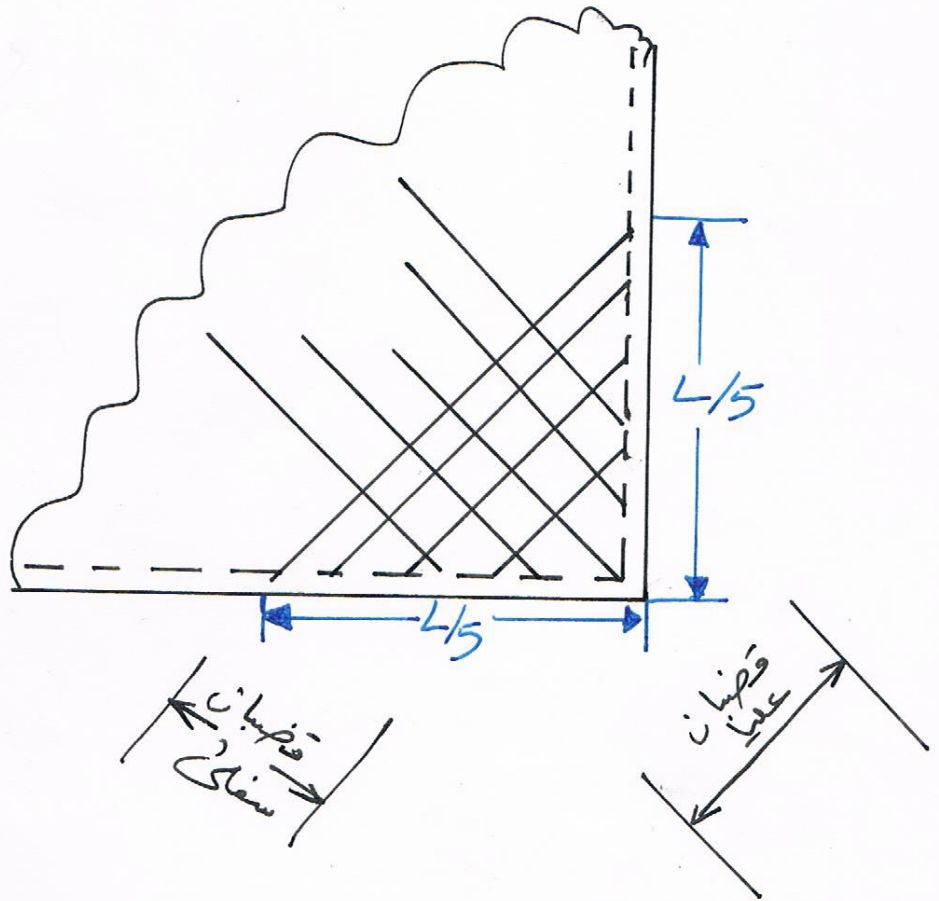
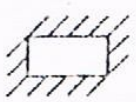
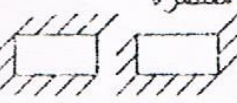

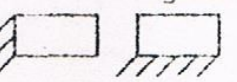
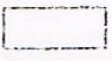


Table (1) ١٥

نوع البلاطة	العزوم	الاتجاه التصير						الاتجاه الطويل لجميع قيم (m)
		نسبة العرض الى الطول (m)						
		1.0	0.9	0.8	0.7	0.6	0.5	
بلاطة داخلية 	$M_{\bar{u}cont}$	0.033	0.040	0.048	0.055	0.063	0.083	0.033
	$M_{\bar{u}disc}$	-----	-----	-----	-----	-----	-----	-----
	M_u^+	0.025	0.030	0.036	0.041	0.047	0.062	0.025
أحد الحافات غير مستمرة 	$M_{\bar{u}cont}$	0.041	0.048	0.055	0.062	0.069	0.085	0.041
	$M_{\bar{u}disc}$	0.021	0.024	0.027	0.031	0.035	0.042	0.021
	M_u^+	0.031	0.036	0.041	0.047	0.052	0.064	0.031
حافتان غير مستمرة 	$M_{\bar{u}cont}$	0.049	0.057	0.064	0.071	0.078	0.09	0.049
	$M_{\bar{u}disc}$	0.025	0.028	0.032	0.036	0.039	0.045	0.025
	M_u^+	0.037	0.043	0.048	0.054	0.059	0.068	0.037
ثلاث حافات غير مستمرة 	$M_{\bar{u}cont}$	0.058	0.066	0.074	0.082	0.090	0.098	0.058
	$M_{\bar{u}disc}$	0.029	0.033	0.037	0.041	0.045	0.049	0.029
	M_u^+	0.044	0.050	0.056	0.062	0.068	0.074	0.044
جميع الحافات غير مستمرة 	$M_{\bar{u}cont}$	-----	-----	-----	-----	-----	-----	-----
	$M_{\bar{u}disc}$	0.033	0.038	0.043	0.047	0.053	0.055	0.033
	M_u^+	0.050	0.057	0.064	0.072	0.080	0.083	0.050

ملاحظات

1- النهاية المؤشرة يقصد بها مستمرة

2- الرموز $M_{\bar{u}cont}$ = العزم السالب للنهاية المستمرة .

$M_{\bar{u}disc}$ = العزم السالب للنهاية غير المستمرة

M_u^+ = العزم الموجب .

Design of Two-Way Slabs :-

* If $\frac{L}{S} < 2.0$, The slabs should be designed as two-way slab.

* There are many kinds of two-way slab like:-

1- Slabs supported by shallow beams.

2- Flat Plate Slabs.

3- Flat Slabs :-

a- Flat slabs with drop panels.

b- Flat slab with column capital.

c- Slab with drop panel & capital.

4- Two way ribbed slabs.

Design of Edge Supported Slabs :-

* There are three methods for design this type of slab

* We will use the second method for the design.

