Optimization Modeling

Water Users:

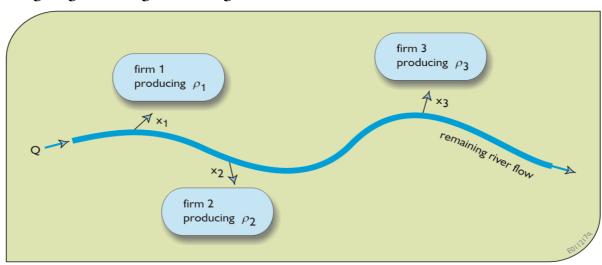
- Allocate release Q to 3 users and provide instream flow S
- Net-benefit from allocation of x_i

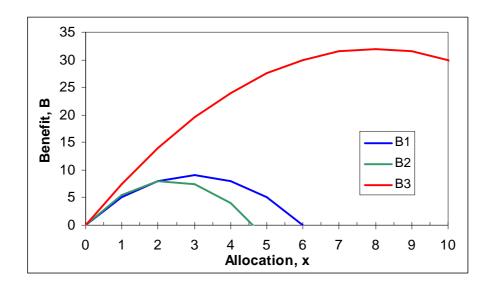
$$B_{i}(x_{i}) = a_{i}x_{i} - b_{i}x_{i}^{2}$$
 $i = 1,2,3$

$$B_{1}(x_{1}) = 6x_{1} - x_{1}^{2}$$

$$B_2(x_2) = 7x_1 - 1.5x_2^2$$

$$B_3(x_3) = 8x_3 - 0.5x_3^2$$





 \blacksquare Decision variables: xi, i=1,2,3

■ Objective:

$$maximize \sum_{i=1}^{3} (a_i x_i - b_i x_i^2)$$

Note: if sufficient water is available the allocations are independent and equal to $x_1^* = 3$, $x_2^* = 2.33$, $x_3^* = 8$

■ Optimization model:

$$maximize \sum_{i=1}^{3} (a_i x_i - b_i x_i^2)$$

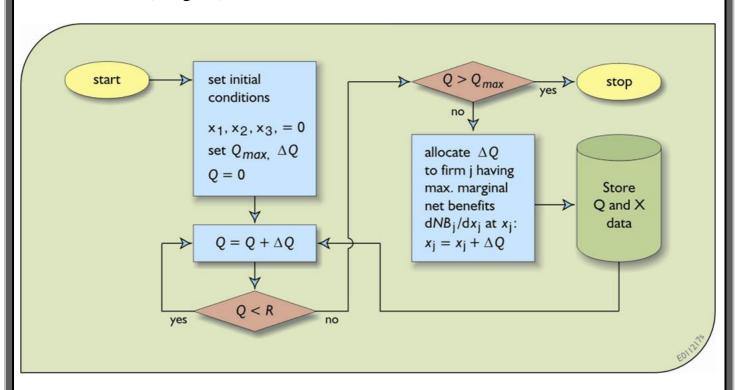
 \boldsymbol{x}

subject to

$$\sum_{i=1}^{3} x_i + R = Q$$

Flowcharting Details

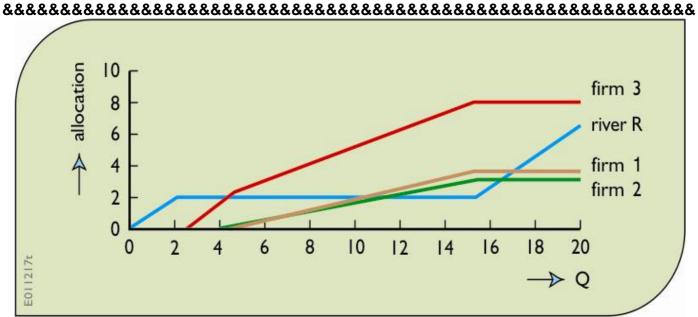
lacktriangle Divide available flow Q into increments and allocate each increment to get maximum additional (marginal) benefit from incremental amount of water



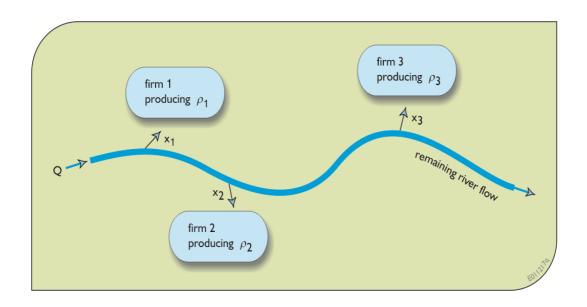
Q	$Q_{max} = 8$; $Q_i = 0$; $\Delta Q = 1$; river flow $R \ge \min \{Q, 2\}$														
										total net benefits					
							7	-3 x	N. 100 C.					Σ_{j}	$NB_{j}(x_{1})$
			R	x ₁	x ₂	x ₃	6-2 x ₁		8-x ₃		R	x ₁	\mathbf{x}_2	x ₃	
	I-3	0-2	0–2	0	0	0	6	7	8	3	2	0	0	1	7.5
	4	3	2	0	0	Ī	6	7	7	4	2	0	0	2	14.0
	5	4	2	0	0	2	6	7	6	5	2	0	Ī	2	19.5
	6	5	2	0	1	2	6	4	6	6	2	0	1	3	25.0
	7	6	2	0	-1	3	6	4	5	7	2	1	-11	3	30.0
	8	7	2	1	1	3	4	4	5	8	2	1	1	4	34.5
	9	8	2	1	1	4	4	4	4	-	* -	-	a - a		

$Q_{max} = 20;$		$\Delta Q \longrightarrow 0$; ri	ver flow	R ≥ min {Q	, 2}	selected v	alues of Q
Q		allocations. R, x_j			margin	al net be	total net benefits	
	R	x ₁	x ₂	x ₃	6-2 x ₁	7-3 x ₂	8- x ₃	$\Sigma_{j} NB_{j}(x_{1})$
0–2	0–2	0	0	0	6	7	8	0.0
4	2	0	0.25	1.75	6.00	6.25	6.25	14.1
5	2	0.18	0.46	2.36	5.64	5.64	5.64	20.0
8	2	1.00	1.00	4.00	4.00	4.00	4.00	34.5
10	2	1.55	1.36	5.09	2.91	2.91	2.91	41.4
15	2	2.91	2.27	7.82	0.18	0.18	0.18	49.1
20	6.67	3.00	2.33	8.00	0	0	0	49.2

Al Anbar University Water Resources Management & Economics Mr. Ahmed A. Al Hity College of Engineering 4th Stage Lecture No: 8 Water Resources and Dams Dept. 2019-2020 Date: Wed.22/04/2020



Example:



♦ Lagrangean

$$L(\vec{x},\lambda) = \sum_{i=1}^{3} (a_i x_i - b_i x_i^2) - \lambda \left(\sum_{i=1}^{3} x_i + R - Q\right)$$

◆ First – order conditions

$$\frac{\partial L}{\partial x_1} = a_1 - 2b_1 x_1 - \lambda = 0$$

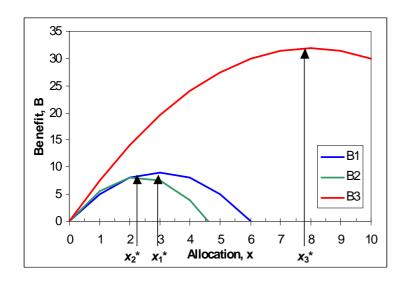
$$\frac{\partial L}{\partial x_2} = a_2 - 2b_2 x_2 - \lambda = 0$$

$$\frac{\partial L}{\partial x_3} = a_3 - 2b_3 x_3 - \lambda = 0$$

$$\frac{\partial L}{\partial \lambda} = x_1 + x_2 + x_3 + R - Q = 0$$

$$x_{i}^{*} = \frac{a_{i} - \lambda}{2b_{i}} \qquad i = 1, 2, 3$$

$$\lambda^{*} = \frac{2\left(\sum_{i=1}^{3} \frac{a_{i}}{2b_{i}} + R - Q\right)}{\sum_{i=1}^{3} \frac{1}{b_{i}}}$$



$$B_i(x_i) = a_i x_i - b_i x_i^2$$
 $i = 1,2,$

$$a_1 = 6$$
; $a_2 = 7$; $a_3 = 8$
 $b_1 = 1.0$; $b_2 = 1.5$; $b_3 = 0.5$

Total

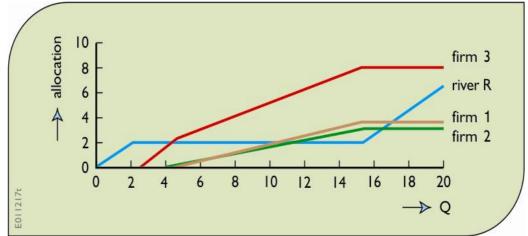
Equal marginal benefits (slopes) for all users

$$\lambda = \frac{\partial NB}{\partial Q} = \frac{\partial B_i}{\partial x_i}$$

						Downstream
$\boldsymbol{\varrho}$	x_1	x_2	x_3	λ	R	Flow
5.00	0.18	0.45	2.36	5.64	2.00	2.00
8.00	1.00	1.00	4.00	4.00	2.00	2.00
10.00	1.55	1.36	5.09	2.91	2.00	2.00
15.00	2.91	2.27	7.82	0.18	2.00	2.00
16.00	3.00	2.33	8.00	0.00	2.00	2.67
20.00	3.00	2.33	8.00	0.00	2.00	6.67

Release Allocation Rule

Rule tells you the amount of released water allocated to each use



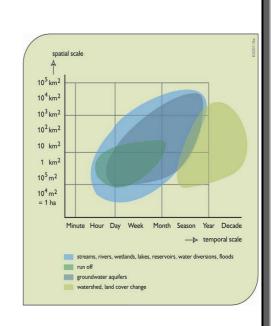
River Basin Modeling

Water Resources

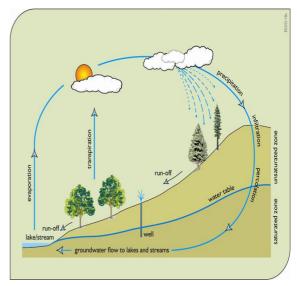
- ♦ Water at:
 - Wrong place, wrong quantity, wrong time
- ◆ What to do?
- ◆ Manipulate the hydrologic cycle
 - Build facilities? Remove facilities? Reoperate facilities?
 - **♦** Reservoirs
 - **♦** Canals
 - ◆ Other infrastructure

Scales of Processes Time Scales

- ◆ Water management plans
 - Consider average conditions within discrete time periods
 - ◆ Weekly, monthly or seasonal
 - Over a long time horizon
 - ◆ Year, decade, century
 - Shortest time period
 - ◆ No less than travel time from the upper basin to mouth
 - ◆ For shorter time periods some kind of flow routing required
- ♦ Flood management
 - Conditions over much shorter periods
 - ♦ Hours, Days, Week



- Precipitation
- Runoff
- **♦** Infiltration
- **♦** Percolation
- **♦** Evapotranspiration
- ◆ Chemical concentration
- **♦** Groundwater



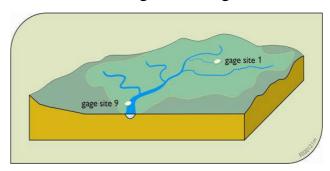
Hydrologic Models

- ◆ Precipitation runoff models
 - Predict runoff from land areas, infiltration into soils, and percolation into aquifers
 - Used when stream gage data are not available, not reliable, or not representative of natural flow conditions (including climate change conditions)
 - Estimate impacts of changing land uses on temporal and spatial distribution of runoff
- ◆ Model characteristics
 - Theoretical or Empirical
 - Deterministic or Stochastic
 - Event-based or Continuous-time
 - Lumped or Distributed

Streamflow Data

- Measurement
- Data sources
- ◆ Flow conditions
 - Natural
 - Present
 - Unregulated
 - Regulated
 - Future

- Reservoir losses
- Missing data
 - Precipitation-runoff models
 - Stochastic streamflow models
 - Extending and filling in historic records



Flows at Ungaged Sites

- lack Have streamflows qtg at gauge sites g = 1 and 9
- ◆ Use these to estimate flows at other sites
- ◆ When runoff per unit land area can be assumed constant over space
 - For a gauge site g, runoff per unit area can be calculated by dividing the gauge flow by the upstream drainage area,

$$q_t^g = \frac{Q_t^g}{A_g}$$

- the estimated streamflow at site s will be

$$Q_t^s = \left(\frac{Q_t^g}{A_g}\right) A_s$$

- ◆ Multiple gauge sites
 - estimated streamflow at ungauged site s is weighted linear combination of unit runoffs times contributing area at site s
- **♦** where
 - *Qst* flow at ungaged site
 - As upstream drainage area
 - g gage site
 - *Qgt* gage flow
 - Ag gage drainage area
 - wg weights
- ◆ *Incremental flow* difference between the natural streamflows at any two sites is called the

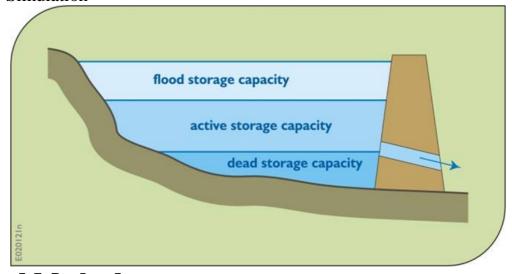
$$Q_t^s = \sum_g w_g \frac{Q_t^g}{A_g} A_g$$

Yield of a System

- ◆ <u>Yield</u> amount of water that can be supplied during some time interval
- Firm yield amount of water that can be supplied in a critical period
 - Without storage: firm yield is lowest streamflow on record,
 - With storage: firm yield can be increased to approximately the mean annual flow of stream

Increase Firm Yield Add storage

- ◆ To increase the firm yield of a stream, impoundments are built. Need to develop the storage-yield relationship for a river
- ◆ Simplified methods
 - Mass curve (Rippl) method
 - Sequent peak method
- ◆ More complex methods
 - Math Programming
 - Simulation



Simplified Methods

- ◆ Mass curve (Rippl) method
 - Graphical estimate of storage required to supply given yield
 - Constructed by summing inflows over period of record and plotting these versus time and comparing to demands
- ◆ Time interval includes "critical period"
 - Time over which flows reached a minimum
 - Causes the greatest drawdown of reservoir

Rippl method

- lacktriangle Find the maximum cumulative difference between reservoir releases Rt and inflows \mathfrak{Q}_t
- lacktriangle Assuming constant reservoir release, \mathcal{R}_{b} in each period t
 - A line with slope \mathcal{R}_t is placed tangent to the
 - cumulative inflow curve.
 - To the right the release R_t exceeds the inflow Q_t

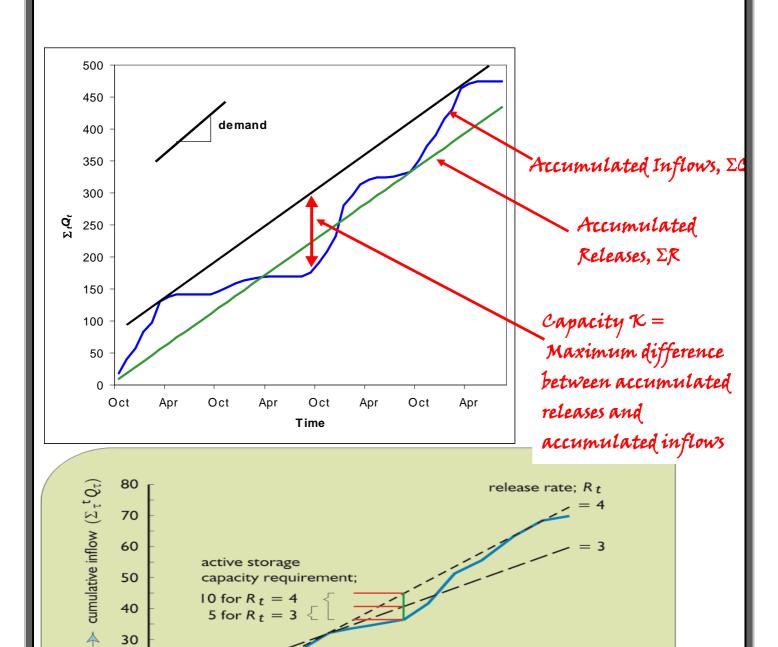
- The maximum vertical distance between the cumulative inflow curve and the release line equals the maximum water deficit
- This is the required active storage capacity

$$K_a = \text{maximum} \left[\sum_{t=i}^{j} (R_t - Q_t) \right]$$

where $1 \le i \le j \le 2T$.



t	Q(t)	$\Sigma Q(t)$	R(t)	$\Sigma R(t)$	t	Q(t)	$\Sigma Q(t)$	R(t)	$\Sigma R(t)$
Oct	18	18	9.3	9.3	Apr	1	169	9.3	175.8
Nov	22	40	9.3	18.5	May	0	169	9.3	185.0
Dec	17	57	9.3	27.8	Jun	0	169	9.3	194.3
Jan	26	83	9.3	37.0	Jul	0	169	9.3	203.5
Feb	15	98	9.3	46.3	Aug	0	169	9.3	212.8
Mar	32	130	9.3	55.5	Sep	7	176	9.3	222.0
Apr	8	138	9.3	64.8	Oct	15	191	9.3	231.3
May	3	141	9.3	74.0	Nov	17	208	9.3	240.5
Jun	0	141	9.3	83.3	Dec	25	233	9.3	249.8
Jul	0	141	9.3	92.5	Jan	47	280	9.3	259.0
Aug	0	141	9.3	101.8	Feb	16	296	9.3	268.3
Sep	0	141	9.3	111.0	Mar	18	314	9.3	277.5
Oct	5	146	9.3	120.3	Apr	7	321	9.3	286.8
Nov	6	152	9.3	129.5	May	4	325	9.3	296.0
Dec	6	158	9.3	138.8	Jun	0	325	9.3	305.3
Jan	5	163	9.3	148.0	Jul	1	326	9.3	314.5
Feb	3	166	9.3	157.3	Aug	3	329	9.3	323.8
Mar	2	168	9.3	166.5	Sep	4	333	9.3	333.0



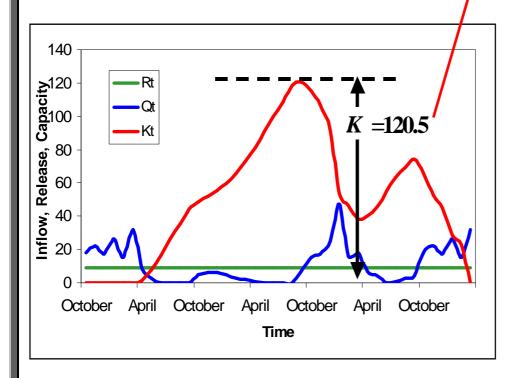
Sequent Peak Method

- \bullet Plot cumulative inflows, Qt, minus releases, Rt
- ◆ Note first peak and the sequent peak (next peak that is greater than first)

 \rightarrow time t

- ◆ Required storage is vertical difference between first peak and low point before sequent peak
- ◆ Largest value of storage is design value

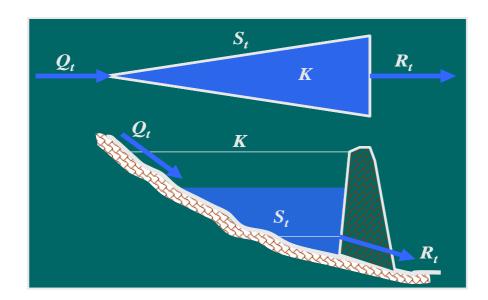
t	R_t	Q_t	K_{t-1}	K_t
October	9.25	18	0.0	0.0
November	9.25	22	O.O	0.0
December	9.25	17	0.0	0.0
January	9.25	26	0.0	0.0
February	9.25	15	0.0	0.0
March	9.25	32	0.0	0.0
April	9.25	8	0.0	1.3
May	9.25	3	1.3	7.5
• • •	• • •	• • •		
May	9.25	O	81.3	90.5
June	9.25	O	90.5	99.8
July	9.25	O	99.8	109.0
August	9.25	O	109.0	118.3
September	9.25	7	118.3	120.5
October	9.25	15	120.5	114.8
November	9.25	17	114.8	107.0
December	9.25	25	107.0	91.3
• • •	• • •	• • •		
January	9.25	26	45.3	28.5
February	9.25	15	28.5	22.8
March	9.25	32	22.8	0.0



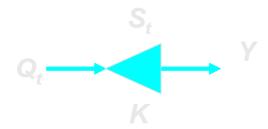
Seque
$$K_{t} = \begin{cases} R_{t} - Q_{t} + K_{t-1} & \text{If } R_{t} - Q_{t} + K_{t-1} \ge 0 \\ 0 & \text{If } R_{t} - Q_{t} + K_{t-1} < 0 \end{cases}$$

time t	$(R_t -$	Q _t +	K _{t-1}) ⁺ =	K _t
1	3.5 -	- 1.0 -	0.0	=	2.5
2	3.5 -	3.0	- 2.5	=	3.0
3	3.5 -	3.0	- 3.0	=	3.5
4	3.5 -	5.0	3.5	=	2.0
5	3.5 -	8.0	- 2.0	=	0.0
6	3.5 -	6.0	0.0	=	0.0
7	3.5 -	7.0	0.0	=	0.0
8	3.5 -	2.0	0.0	=	1.5
9	3.5 -	- 1.0 -	1.5	=	4.0
1	3.5 -	- 1.0 -	+ 4.0	=	6.5
2	3.5 -	3.0	6.5	=	7.0
3	3.5 -	3.0	7.0	=	7.5
4	3.5 -	5.0	7.5	=	6.0
5	3.5 -	8.0	6.0	=	1.5
6	3.5 -	- 6.0 -	⊦ 1.5	=	0.0
7	3.5 -	7.0	0.0	=	0.0
8	3.5 -	2.0	0.0	=	1.5
9	3.5 -	- 1.0 -	- 1.5	=	4.0

Reservoir



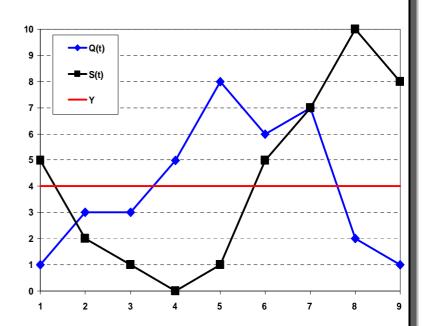
Maximize yield (Y), Given capacity (K)



- ◆ Maximize constant release given capacity and inflows
 - Ot Inflows to the reservoir
 - St Storage volumes in the reservoir
 - Y Constant release (yield) from the reservoir
 - K Capacity of the reservoir

Maximize Y Fined subject to $S_t + Q_t - Y = S_{t+1} \qquad t = 1, ..., T; \ T+1=1$ $S_t \leq K \qquad t = 1, ..., T$ Given

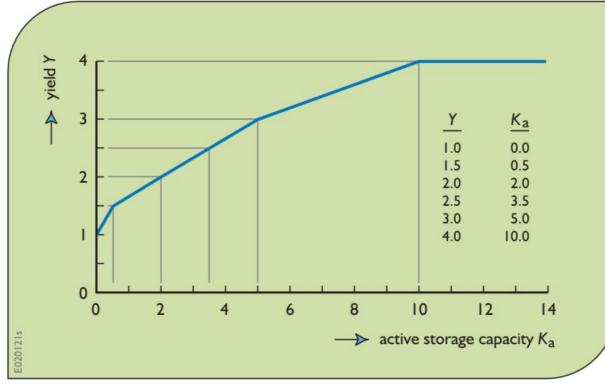
Inflow	Storage	Yield
Q(t)	S(t)	Y
1.00	5.00	4.00
3.00	2.00	4.00
3.00	1.00	4.00
5.00	0.00	4.00
8.00	1.00	4.00
6.00	5.00	4.00
7.00	7.00	4.00
2.00	10.00	4.00
1.00	8.00	4.00



Maximize *Y* subject to

$$\begin{split} S_{t+1} \leq S_t + Q_t - Y & t = 1, ..., T; \ T+1 = 1 \\ S_t \leq K & t = 1, ..., T \end{split}$$

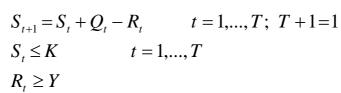
Capacity – Yield Function



Max K, Given Y

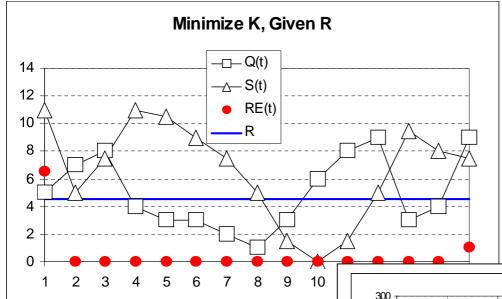
◆ Maximize constant release given capacity and inflows

Minimize *K* subject to



K

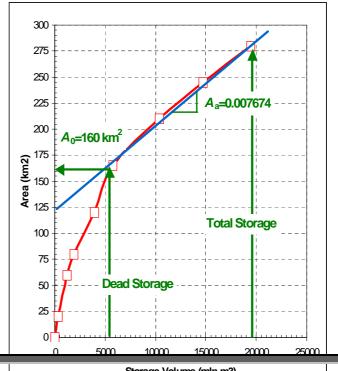
	Inflow	Storage	Release	Yield
t	Q(t)	S(t)	RE(t)	R
1	5	11	6.5	4.5
2	7	5	0	4.5
3	8	7.5	0	4.5
4	4	11	0	4.5
5	3	10.5	0	4.5
6	3	9	0	4.5
7	2	7.5	0	4.5
8	1	5	0	4.5
9	3	1.5	0	4.5
10	6	0	0	4.5
11	8	1.5	0	4.5
12	9	5	0	4.5
13	3	9.5	0	4.5
14	4	8	0	4.5
15	9	7.5	1	4.5



Evaporation

$$S_{t+1} = S_t + Q_t - R_t - L_t$$

- Lt Losses from reservoir
- A Surface area of reservoir
- et ave. evaporation rate



Storage Volume (mln m3)

$$\begin{split} L_{t} &= \left[A_{a} \overline{S}_{t} + A_{0} \right] e_{t} \\ &= \left[A_{a} \left(\frac{S_{t} + S_{t+1}}{2} \right) + A_{0} \right] e_{t} \\ &= A_{a} e_{t} \left(\frac{S_{t} + S_{t+1}}{2} \right) + A_{0} e_{t} \\ &= 0.5 A_{a} e_{t} S_{t} + 0.5 A_{a} e_{t} S_{t+1} + A_{0} e_{t} \\ &= a_{t} S_{t} + a_{t} S_{t+1} + b_{t} \end{split}$$

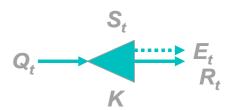
$$S_{t+1} = S_t + Q_t - R_t - L_t$$

$$L_t = a_t S_t + a_t S_{t+1} + b_t$$

$$S_{t+1} = S_t + Q_t - R_t - (a_t S_t + a_t S_{t+1} + b_t)$$

$$(1+a_t)S_{t+1} = (1-a_t)S_t + Q_t - R_t - b_t$$

Reservoir with Power Plant Power Production



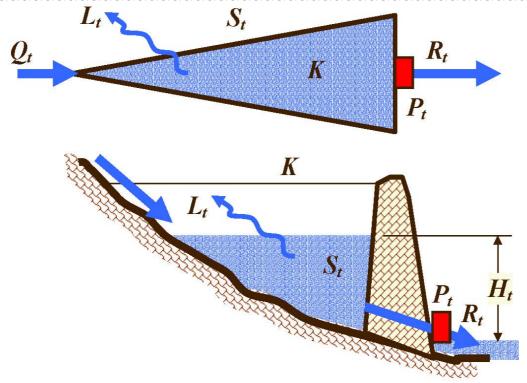


Figure 3.1.1. Diagram of reservoir system.

Qt = Inflows (mln.m³/period)

St = Storage volume (mln.m³)

 $K = \text{Capacity (mln.m}^3)$

Rt = Release (mln.m³/period)

Et = Energy (kWh)

Ht = Head(m)

k =coefficient (efficiency, units)

$$\overline{H}_t = \frac{H(S_t) + H(S_{t+1})}{2} \quad \text{m}$$

$$q_t = R_t * 10^6 / time_t \text{ m}^3 / \text{sec}$$

$$P_{t} = (9.81)\varepsilon\overline{H}.a.$$

 $E_{t} = P_{t} * time(t) / 3600$

$$E_t = 2730 * \varepsilon \overline{H}_t R_t$$
 kWh

$$E_{t} = 1.024 * \varepsilon \overline{H}_{t} R_{t}$$
 kWh

H in ft

R in acre-feet

Maximize
$$\sum_{t=1}^{T} E_t$$

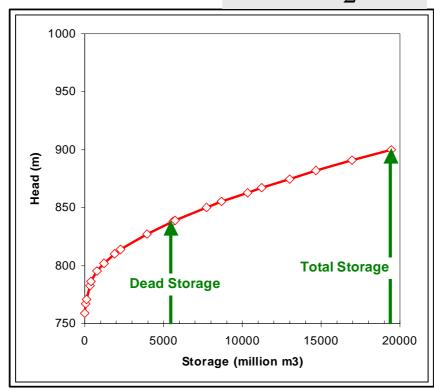
subject to

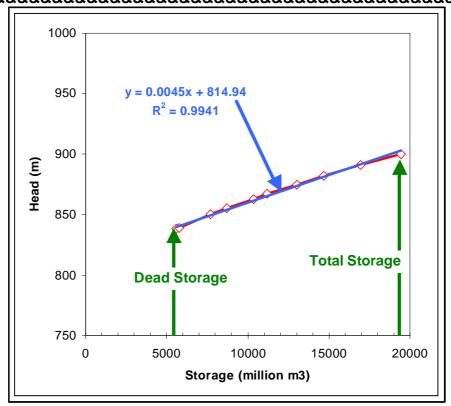
$$\begin{split} S_t + Q_t - R_t &= S_{t+1} \\ S_t &\leq K \\ \overline{H}_t &= \frac{H(S_t) + H(S_{t+1})}{2} \\ E_t &= k \overline{H}_t R_t \end{split}$$

$$t = 1, ..., T$$

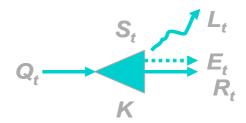
Head vs Storage Relation

$$\overline{H}_t = \frac{H(S_t) + H(S_{t+1})}{2}$$





Model



Minimize
$$\sum_{t=1}^{T} (R_t - D_t)^2$$

subject to

$$(1+a_{t})S_{t+1} = (1-a_{t})S_{t} + Q_{t} - R_{t} - b_{t}$$

$$S_{t} \leq K \qquad t = 1,...,T$$

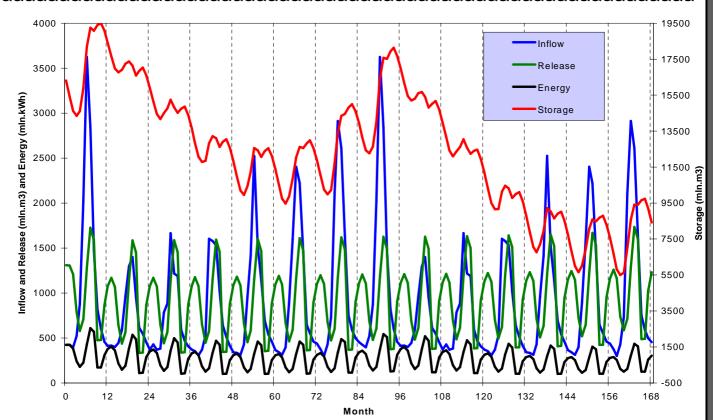
$$H_{t} = H_{o} + cS_{t}$$

$$\overline{H}_{t} = \frac{(H_{t} - H_{o}) + (H_{t+1} - H_{o})}{2}$$

$$q_{t} = R_{t} * 10^{6} / time_{t} \leq q_{\text{max}}$$

$$P_{t} = (9.81)\varepsilon \overline{H}_{t} q_{t} \leq P_{\text{max}}$$

$$E_{t} = P_{t} * time(t) / 3600$$



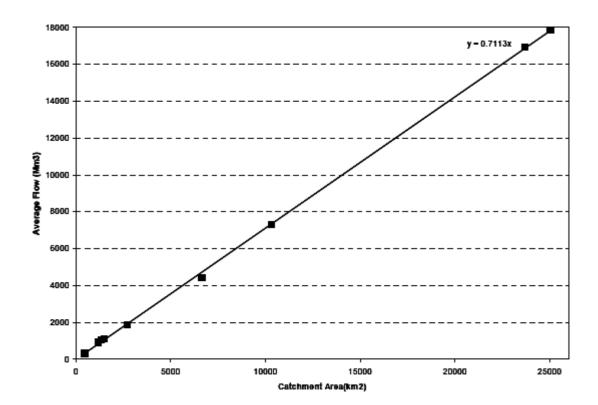
Example1: Using the following information pertaining to the drainage area and discharge in the Han River in South Korea, verify the equation

$$Q_t^s = \sum_{\mathbf{g}} w_{\mathbf{g}} \, \frac{Q_t^{\mathbf{g}}}{A_{\mathbf{g}}} A_s$$

for predicting the unregulated flow at any site in the river, by plotting the average flow as a function of catchments area. What does the slope of the line equal?

Gage Point	Catchment Area (km2)	Average Flow (million m3/yr)
First Bridge	25047	17860
Pal Dang	23713	16916
So Yang	2703	1856
Chung Ju	6648	4428
Yo Ju	10319	7300
Hong Chun	1473	1094
Dal Chung	1348	1058
Kan Yun	1180	926
Im Jae	461	316

ANSWER--A plot of the average flow Q as a function of the catchments area A upstream of each site s shows an essentially constant slope. This indicates that the flow runoff per unit catchments area is approximately constant throughout the watershed, as assumed by the equation.



Example2: Compute the storage-yield function for a single reservoir by the sequent peak method given the following sequence of inflows: (7,3,5,1,2,5,6,3,4). Next assume that each year has two distinct hydrologic seasons, one wet and one dry, and that 80% of the inflow occurs in the wet season and 80% of the yield is desired in the dry season. Using the sequent peak method, show the increase in storage capacity required for the same annual yield resulting from the within-year

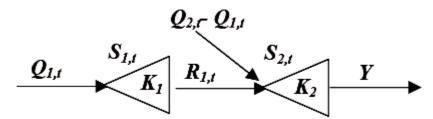
redistribution requirements.

ANSWER

Single Seas	on			Dual Season					
t	R	Q	K-1	K	t	R	Q	K-1	K
1	3.5	7	0	0	11	0.7	5.6	0	0
2	3.5	3	0.5	0	12	2.8	1.4	0	1.4
3	3.5	5	0	0.5	21	0.7	2.4	1.4	0
4	3.5	1	2.5	0	22	2.8	0.6	0	2.2
5	3.5	2	4	2.5	31	0.7	4.0	2.2	0
6	3.5	5	2.5	4	32	2.8	1.0	0	1.8
7	3.5	6	0	2.5	41	0.7	8.0	1.8	1.7
8	3.5	3	0.5	0	42	2.8	0.2	1.7	4.3
9	3.5	4	0	0.5	51	0.7	1.6	4.3	3.4
					52	2.8	0.4	3.4	5.8
					61	0.7	4.0	5.8	2.5
					62	2.8	1.0	2.5	4.3
					71	0.7	4.8	4.3	0.2
					72	2.8	1.2	0.2	1.8
					81	0.7	2.4	1.8	0.1
					82	2.8	0.6	0.1	2.3
					91	0.7	3.2	2.3	0
					92	2.8	8.0	0	2
Capacity	K=			4					5.8

Singl	e Season	Dua	al Season	Increase	
Yield	Capacity	Yield	Capacity	Yields	
1	0	1	0.6	0.2	0.6
				0.8	
2	1	2	1.6	0.4	0.6
				1.6	
3	3	3	4.4	0.6	1.4
				2.4	
3.5	4	3.5	5.8	0.7	1.8
				2.8	
4	5	4	7.2	8.0	2.2
				3.2	

Example3: Construct an optimization model for estimating the least-cost combination of active storage capacities, K1 and K2, of two reservoirs located on a single stream, used to produce a constant flow or yield downstream of the two reservoirs. Assume that the cost functions Cs(Ks) at each reservoir site s are known and there is no dead storage and no evaporation. Assume that 10 years of monthly unregulated flows are available at site s. The system diagram is as shown in Figure



where Q1,t and Q2,t are the unregulated streamflows at sites 1 and 2, respectively, Q2,t - Q1,t is the incremental inflow between site 1 and site 2, R1,t is the release from the upstream reservoir, and Y is the constant yield from the downstream reservoir, S1,t., and S1,t are the reservoir storages, and K1 and K2 are the reservoir capacities.

The model can be formulated as:

Minimize
$$C_1(K_1) + C_2(K_2)$$

 $S_{t,v}^2 \leq K_2$

subject to

$$S_{t,y}^{1} + Q_{t,y}^{1} - R_{t,y}^{1} = S_{t+1,y}^{1}$$
 $\forall t, y$
$$S_{t,y}^{1} \le K_{1}$$
 $\forall t, y$
$$S_{t,y}^{2} + (Q_{t,y}^{2} - Q_{t,y}^{1}) + R_{t,y}^{1} - Y = S_{t+1,y}^{2}$$
 $\forall t, y$

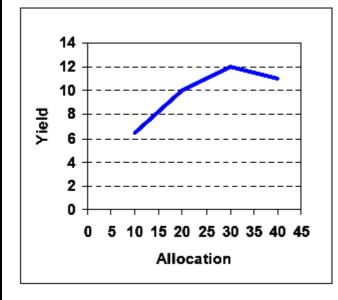
The constant yield *Y* is fixed and all the inflows are known. When t = 12, t+1 = 1 and *y* is y+1. If y = 10, y+1 = 1.

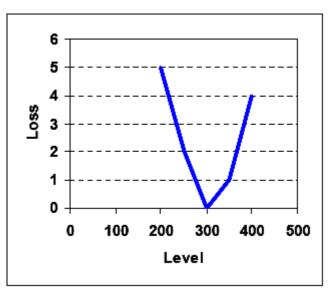
 $\forall t, v$

Example4: Plot the following data on possible recreation losses and irrigated agricultural yields. Show that use of the expected storage level or expected allocation underestimates the expected value of reservoir losses while it overestimates the expected value of crop yield.

Irrigation Water Allocation	Crop Yield/Hectare	Probability of Allocation		
10	6.5	0.20		
20	10.0	0.30		
30	12.0	0.30		
40	11.0	0.20		

Summer storage level	Decrease in recreation benefits	Probability of storage level
200	5	0.10
250	2	0.20
300	0	0.40
350	1	0.20
400	4	0.10





Expected Allocation = ABar = 25; Yield(ABar) = 11 Expected Yield = 10.1 < 11

Expected Level = LBar = 300; Loss(LBar) = 0 Expected Loss = 1.5 > 0